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FILING DATE: *February 10, 2003*
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12/31/02 JC843 U.S. PTO

PTO/SB/16 (8-10)
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PROVISIONAL APPLICATION FOR PATENT COVER SHEET

This is a request fro filing a PROVISIONAL APPLICATION FOR PATENT under 37 CFR 1.53 (c).

JC678 U.S. PTO 60/437140

INVENTOR(S)		
Given Name (first and middle [if any])	Family Name or Surname	Residence (City and either State or Foreign Country)
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☐ *Additional inventors are being named on the ___ separately numbered sheets attached hereto*

TITLE OF THE INVENTION (280 characters max)

LOW PRESSURE DROP DEEP ELECTRICALLY ENHANCED FILTER

Direct all correspondence to: CORRESPONDENCE ADDRESS

■ Customer.Number 008-439 → Place Customer Number Bar Code Label here

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■ Firm or Individual Name	ROBERT E. BUSHNELL & LAW FIRM				
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ENCLOSED APPLICATION PARTS (*check all that apply*)

■ Specification *Number of Pages* 51
■ Drawing(s) *Number of Sheets*: 20
☐ Application Data Sheet. See 37 CFR 1.76
☐ CD(s), Number ______
☐ Other (specify): ______

METHOD OF PAYMENT OF FILING FEES FOR THIS PROVISIONAL APPLICATION FOR PATENT (*check one*)

■ Applicant claims SMALL ENTITY status. See 37 CFR 1.27.
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The invention was made by an agency of the United States Government or under a contract with an agency of the United States Government.
■ No
☐ Yes, the name of the U.S. Government agency and the Government contract number are: ______

Respectfully submitted,
SIGNATURE [signature]
Date: 12/31/02
REGISTRATION NO.: 27,774
(if appropriate)
TYPE or PRINTED NAME: Robert E. Bushnell, Esq.
TELEPHONE: (202) 408-9040
Docket Number: P56855P

USE ONLY FOR FILING A PROVISIONAL APPLICATION FOR PATENT

This collection of information is required by 37 CFR 1.51. The information is used by the public to file (and by the PTO to process) a provisional application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 8 hours to complete, including gathering, preparing, and submitting the complete c\provisional application to the PTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this from and/or suggestions fro reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S.> Department of Commerce, Washington, D.C. 20231. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Box Provisional Application, Assistant Commissioner for Patents, Washington, D.C., 20231.

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FEE TRANSMITTAL

Patent fees are subject to annual revision.

Complete If Known	
Application Number	*to be assigned*
Filing Date	31 December 2002
First Named Inventor	RAJAN JAISINGHANI
Examiner Name	*to be assigned*
Group/Art Unit	*to be assigned*
Attorney Docket No.	P56855P

TOTAL AMOUNT OF PAYMENT ($) 80.00

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1. ☐ The Commissioner is hereby authorized to charge indicated fees and credit any over payments to:

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☐ Charge Any Additional Fee Required Under 37 C.F.R. §1.16 and 1.17.

☐ Applicant claims small entity status. See 37 CFR 1.27

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FEE CALCULATION

1. BASIC FILING FEE

Large Entity Fee Code	Large Entity Fee ($)	Small Entity Fee Code	Small Entity Fee ($)	Fee Description	Fee Paid
1001	740	2001	370	Utility filing fee	$
1002	330	2002	165	Design filing fee	$
1003	510	2003	255	Plant filing fee	$
1004	740	2004	370	Reissue filing fee	$
1005	160	2005	80	Provisional filing fee	$

SUBTOTAL (1) ($) .00

2. EXTRA CLAIM FEES

		Extra Claims		Fee from below		Fee Paid
Total claims	-20** =		x		=	
Independent Claims	- 3** =		x		=	
Multiple Dependent					=	

*** or number previously paid, if greater; For Reissues, see below*

Large Entity Fee Code	Large Entity Fee ($)	Small Entity Fee Code	Small Entity Fee ($)	Fee Description
1201	84	2201	42	Independent claims in excess of 3
1202	18	2202	9	Claims in excess of 20
1203	280	2203	140	Multiple dependent claim, if not paid
1204	84	2204	42	** Reissue independent claims over original patent
1205	18	2205	9	** Reissue claims in excess of 20 and over original patent

SUBTOTAL (2) ($) 0.00

FEE CALCULATION (continued)

3. ADDITIONAL FEES

Large Entity Fee Code	Large Entity Fee ($)	Small Entity Fee Code	Small Entity Fee ($)	Fee Description	Fee Paid
1051	130	2051	65	Surcharge-late filing fee or oath	$
1052	50	2052	25	Surcharge-late provisional filing fee or cover sheet	$
1053	130	1053	130	Non-English specification	$
1812	2,520	1812	2,520	For filing a request for reexamination	$
1804	920*	1804	920*	Requesting publication of SIR prior to Examiner action	$
1805	1,840*	1805	1,840*	Requesting publication of SIR after Examiner action	$
1251	110	2251	55	Extension for reply within first month	$
1252	400	2252	200	Extension for reply within second month	$
1253	920	2253	460	Extension for reply within third month	$
1254	1,440	2254	720	Extension for reply within fourth month	$
1255	1,960	2255	950	Extension for reply within fifth month	$
1401	320	2401	160	Notice of Appeal	$
1402	320	2402	160	Filing a brief in support of an appeal	$
1403	280	2403	140	Request for oral hearing	$
1451	1,510	1451	1,510	Petition to institute a public use proceeding	$
1452	110	2452	55	Petition to revive - unavoidable	$
1453	1,280	2453	640	Petition to revive - unintentional	$
1501	1,280	2501	640	Utility issue fee (or reissue)	$
1502	460	2502	230	Design issue fee	$
1503	620	2503	310	Plant issue fee	$
1460	130	1460	130	Petitions to the Commissioner	$
1807	50	1807	50	Processing fee for provisional applications	$
1806	180	1806	180	Submission of Information Disclosure Statement	$
8021	40	8021	40	Recording each patent assignment per property (Times number of properties)	$
1809	740	2809	370	Filing a submission after final rejection (37 C.F.R. §1.129(a))	$
1810	740	2810	370	For each additional invention to be examined (37 C.F.R. §1.129(b))	$

Other Fee (specify) 2005 Provisional application filing fee $80.00

Other Fee (specify) ________ $

** Reduced by Basic Filing Fee Paid

SUBTOTAL (3) $80.00

SUBMITTED BY				Complete (if applicable)	
Typed or Printed Name	Robert E. Bushnell, Esq.			Reg. Number	27,774
Signature	R. Bushnell	Date	31 December 2002	Deposit Account User ID	

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TITLE

LOW PRESSURE DROP DEEP ELECTRICALLY ENHANCED FILTER

CLAIM FOR PRIORITY

This application makes reference to, claims all benefits inuring under 35 U.S.C. §111(b) from, and incorporates herein my provisional patent application entitled *Low Pressure Drop Deep Electrically Enhanced Filter* earlier filed in the United States Patent and Trademark Office on the 12th day of July 2002 and there duly assigned Serial No. 60/395,324.

BACKGROUND OF THE INVENTION

Technical Field

[0002] This application pertains to filters and filtration processes generally and, more particularly, to enabling the use of deep filter media used in ionizing electrically enhanced filtration processes and filters while functioning as high performance devices with ultra-low pressure drop.

Related Art

[0003] Jaisinghani, *A Safe Ionizing Field Electronically Enhanced Filter and Process For Safely Ionizing A Field Of An Electrically Enhanced Filter* U.S. Patent No. 5,403,383, describes an ionizing electrically enhanced filter that has sufficiently high performance to have become the only successfully commercialized Electrically Enhanced Filter (*i.e.*, EEF). It has found uses in cleanrooms and in other critical applications, and also in residential and commercial building

applications requiring clean indoor air. Recently, *Consumer Reports* (Feb. 2002) rated a device based on the teachings of this patent as being the highest performance residential air cleaner.

[0004] The main advantages of electrically enhanced filtration technology are high filtration efficiency with low-pressure drop and low resistance to air flow, the safety of these devices constructed with electrically enhanced technology and the ability of these devices to function without problems for the duration of the life of the product; these filters also have some bactericidal properties.

[0005] In contrast, non-EEF type conventional mechanical filters exhibit a higher pressue drop. Embodiments constructed according to the principles of U.S. Patent No. 5,403,383 are limited as a practical matter, to relatively shallow filter media with peak-to-peak depths of about six inches.

[0006] Recent advances in filter construction have resulted in the availability of very low-pressure drop mechanical filters. For example, a class of filters known as mini-pleated V-pack filters have lower pressure drop than older deep filters such as aluminum separator type folded media and other conventional filters. A typical V-pack filter is about twelve inches deep and has a filter efficiency of 99.99% with a particle size of 0.3 micrometers, and has a pressure drop of about one inch water column at a filter face flow velocity of 600 feet per minute. Another grade of such a V-pack filter having a filtration efficiency of 95% at 0.3 micrometers particle size, and has a pressure drop of about one-half of an inch water column (*i.e.*, .05" WC) at a filter face air flow velocity of 600 feet per minute. I have found that if such a 95% filter could be enhanced in a safe electrical manner to provide approximately 99.97 to 99.99% filtration efficiency

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(commonly referred to as HEPA filtration efficiency), then an ultra low pressure drop HEPA filter could be achieved with significant savings in operational costs than are available with conventional HEPA filters. Similarly lower grade, deep V pack or other forms of deep filter material could be safely electrically enhanced to produce higher efficiency filters having significantly lower pressure drops. The operating cost savings would be in terms of fan power required and the longevity of the filter, improvements that result in savings in terms of downtime, labor and material costs related to filter replacement and maintenance. The consequential benefits in industrial applications (cf. Jaisinghani, "*Energy Efficient Cleanroom Design*", 2000) could be as high as 60% savings in energy consumption related to air moving. This would provide a significant reduction in the overall industrial energy consumption required for air moving and heating, ventilating and air conditioning (*i.e.*, HVAC) costs, this provides significant reductions in greenhouse gases and other pollutant associated with energy production.

[0007] Cheney and Spurgin in their *Electrostatically Enhanced HEPA Filter,* U.S. Patent No. 4,781,736 describe an EEF that can be used with deeply folded filter media that has corrugated aluminum separators positioned within the folds. Cheney '736 is limited to using such separators as electrodes within folded dielectric filter media in paper form. The essential objective of Cheney '736 is an attempt to provide electrostatic augmented filtration that allows retrofitting or direct use of existing filters (referring to aluminum corrugated separator deep filters). Cheney '736 requires corrugated separators used as electrodes placed within folded media; if the electrodes in Cheney '736 were flat, those electrodes could not function as separators.

[0007] I have noticed that filters such as those taught by Cheney '736 rely upon sets of spacers

to separate the filter media in an effort to reduce pressure drop and resistance to the air flow. I have found that this undesirably reduces the surface area of filter media available to remove particles from the air flow, principally due to the reliance upon the use of older less efficient aluminum separator folded media filters.

[0008] Embodiments of the Cheney and Spurgin U.S. Patent No. 4,781,736 reference are also restricted to the use of an ionizer that uses parallel plates because the flow is parallel to the air flow direction. I have noticed that there are problems with parallel ionizer plates attributable to dust particles of opposing charge that tend to accumulate on the ionizer plates because the dust particles only have to travel across the direction of the air flow in order to accumulate on the plates. As highly resistive dust builds up on the plates, an opposing field can be generated, thereby canceling the applied field strength that ionizes the air. I have observed that this phenomenon can sometimes generate undesired back corona discharge.

[0009] Cheney '736 also sought a significant reduction in the capacitance of the device in comparison to the teachings of Masuda found in U.S. Patent Nos. 4,357,150 and 4,509,958, in order to minimize the energy available for arcing. Although it is unclear whether this method may reduce the energy available for arcing as compared to Masuda '150 and '958, it reduces neither arcing and the consequent damage to the media nor the potential for fire, because pin holes can be created on the delicate glass media even with low energy arcing. Embodiments of Masuda are highly prone to arcing.

[0010] I have also found that a device constructed in accordance with Cheney '763 lacks a uniform electrical field, exhibits a low collector field strength, demonstrates a high potential for

sparking, tends to have excessive leakage current, and requires construction of its frame from non-conductive materials, as explained in the following discussion.

[0011] Typically, the folded glass fiber media used in filters with aluminum separators in structures such as taught by Cheney '736, is about 0.02" thick. I have found that it is very difficult, if not impossible, to achieve identical folds that is, folds with less than 0.08" variation in thickness and identical corrugated separators, that is, tolerances of corrugation angles and cut lengths that are respectively better than five degrees and lengths better than 0.06". Recognizing that variation in the induced electrical field depends on the least distance d_2 from the ionizing electrode to the upstream corrugated spacers at a fixed applied potential to the wires, when both the tolerances in media folds and aluminum spacers are taken into account, there are concomitantly large and undesirable variations in induced potentials and hence in collection field strength, and therefore erratic filtration performance within various sections of the filter medium. Moreover, the variation in the upstream corrugated spacer alignment with respect to the downstream spacers is responsible for a lack of uniform performance of the filter; the performance will vary from media section to section since the collection field strength will be inversely proportional to the local thickness of the medium. This means that some sections of the filter will have very low enhancement of filtration efficiency. If deeper pleated spacers are used, this situation is worsened.

[0012] A high potential for sparking with contemporary filtering devices occurs because the voltage induced on the upstream electrodes is a function of distance from the ionizing electrode. Keeping in mind that a voltage higher than about 9.35 kilovolts can not be induced on the

upstream electrodes, one can clearly see how daunting the task of maintaining such a precise gap between each and every one of the upstream electrodes and the inducing wire. Since the aluminum separator electrodes are simply placed, unsecured, between the media folds, it is highly likely that some of the electrodes will be too close and cause a higher surface potential on those upstream corrugated electrodes that are closer to the high voltage wire, resulting in corona discharge and sparking at points where the peaks of the upstream and downstream corrugations of the electrodes align. Sparking may burn holes in the filter media and has the potential to cause a fire if the sparking is continuous. In tests that I have done, it was practically impossible to get a filter element that has been constructed with aluminum separators to function without sparking while simultaneously achieving a significant improvement in filtration, especially under higher humidity (*i.e.*, 60% or higher) conditions. Even if an ideal manufacturing method was developed for making filters with aluminum separators separating neighboring layers of the filter medium, contemporary practice is unable to predictably control the distance between corrugated electrodes and the high voltage wire so that no sparking occurred and, at the same time, filtration performance was significantly improved. Moreover, contemporary practice with aluminum separators still results in significant variations in surface potential and, therefore, the strength of collection fields across different portions of the filter.

[0013] Excessive leakage current occurs in contemporary filtering devices because the filter medium is highly porous (*e.g.*, porosity > 95%) and I have found that when the minimum distance between the high voltage wire and the downstream corrugated electrode is not significantly greater than the distance between the wire and the upstream corrugated electrode,

there will be a considerable amount of leakage current towards the downstream corrugated electrode which is at ground potential. This will make the device inefficient. Efficiency is further reduced when the glass filter paper absorbs moisture during occasions of higher humidity.

[0014] In order to prevent sparking towards the frame material, the frame material in the practice of Cheney '736 must be a non-conductive material, typically wood, because the aluminum spacers of the upstream corrugated electrodes will probably contact the frame material at some location. Contemporary manufacturing methods have switched to the use of aluminum or metal channel frames that do not shed particles, provide better seals to the media and are not flammable. The use of organic materials for the frames as suggested by Cheney '736 is rather dirty, and thus undesirable for clean room applications.

[0015] It should be noted that Cheney '736 does not describe any values for electrode gaps or ranges of voltages used in any of the configurations illustrated, nor provide any results showing the efficacy of the embodiments disclosed. These practical difficulties and limitations upon performance are the main reason why such a device such as taught by Cheney '736 has never been successfully commercialized. Additionally, aluminum separator folded filter type filter elements have become unpopular because this type of filter element tends to tear due to the sharp edges of the aluminum separators within the folded medium.

SUMMARY OF THE INVENTION

[0016] It is therefore, an object of the present invention to provide an improved electrically enhanced filtration process and filter.

[0017] It is another object to enable electrically enhanced filtration with a deep filter providing high surface area in a manner that enables use of stable and uniform collection field strengths while suppressing arcing across the filter media.

[0018] It is yet another object to enable electrically enhanced filtration with a deep filter that provides a high surface area in a manner that enables use of stable and uniform collection field strengths in a safe manner.

[0019] It is still another object to enable electrically enhanced filtration with a deep filter that provides a high surface area in a manner that allows the use of stable and uniform collection field strengths by using an ionizer that is not prone to back corona discharge or ionizing field cancellation effects attributable to the collection of highly resistive dust on the ground electrode plate of the ionizer.

[0020] It is still yet another object to enable electrically enhanced filtration with a deep filter that provides a high surface area and allows the use of stable and uniform collection field strength in a manner that it is at least as effective as the filtration achieved by contemporary devices.

[0021] It is a further object to enable high efficiency filtration with very low pressure drops and low resistance to air flow, by electrically enhancing the performance of deep V-pack filter elements.

[0022] It is a yet further object to provide a high efficiency particulate air (i.e., a HEPA filter) with about half the pressure drop of the best currently available deep V-pack HEPA filter element.

[0023] It is a still further object to provide a filter that inhibits growth of microorganisms caught on the filter and that has the potential to actually kill some bacteria entering the filter.

[0024] It is also an object to provide a process for constructing a deep V-pack filter element that can be used as an effective and safe electrically enhanced filter.

[0025] These and other objects may be achieved with a deep V-pack filter element bearing a charge transfer electrode (*i.e.*, a CTE electrode) formed on the obverse side of the filter media and a ground potential electrode formed on the reverse side of the filter media. The filter element may be disposed within the flow of a stream of transient air directed toward the obverse side of the filter medium bearing the charge transfer electrode oriented toward the upstream side of an electrostatically stimulating filtering apparatus, while an ionizer with a single ionizing electrode, or in alternative embodiments, a plurality of ionizing electrodes positioned in an array, is spaced-apart from opposite facing charge transfer electrodes. The ionizing electrode is located between and extends parallel to the exposed surfaces of the control ground electrode and the charge transfer electrode, with the length of the ionizing electrode oriented perpendicular to the direction of the flow of transient air.

BRIEF DESCRIPTION OF THE DRAWINGS

[0026] A more complete appreciation of the invention, and many of the attendant advantages thereof, will be readily apparent as the same becomes better understood by reference to the following detailed description when considered in conjunction with the accompanying drawings in which like reference symbols indicate the same or similar components, wherein:

[0027] Figs. 1a, 1b and 1c respectively show an elevational view of the inlet side, an enlarged elevational view of that outlet side, and an elevational view of an outlet side of an electrically enhanced filter constructed according to the principles of the present invention;

[0028] Figs 2 shows two of the many variations in the alignment of electrodes that are possible in the construction of contemporary filtering devices;

[0029] Fig. 3 is a two coordinate graph illustrating the amplitude of voltage induced on the upstream electrodes as a function of distance between the nearest ionizing electrode and the upstream electrodes;

[0030] Figs. 4 and 5 are schematic diagrams illustrating the necessity for the charge transfer electrode of the electrical enhancement of deep filters as shown by Figure 5, in comparison with contemporary electrically enhanced, relatively shallow filters;

[0031] Fig. 6 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0032] Fig. 7 shows the details of an ionizing electrode mounted with a control ground electrode in an embodiment constructed according to the principles of the present invention;

[0033] Fig. 8 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0034] Fig. 9 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0035] Fig. 10 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0036] Fig. 11 is an enlarged view showing the printed lines that may be formed to serve the charge transfer electrode on the filter element;

[0037] Fig. 12 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0038] Fig. 13 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0039] Fig. 14 shows an alternative configuration of an embodiment constructed according to the principles of the present invention;

[0040] Fig. 15 is an exploded view of ionizer and filter assemblies for use with an electrically enhanced filter constructed according to the principles of this invention;

[0041] Fig. 16 is a two coordinate graph illustrating corona onset occurring as a function of the voltage applied across an ionizing electrode as measured in kilo-Volts and the voltage induced on the charge transfer electrode in kilo-Volts;

[0042] Fig. 17 is an exploded view illustrating two alternate embodiments of filter media elements constructed according to the principles of the invention;

[0043] Fig. 18 is an elevation view illustrating an assembly that can be used to mount single or multiples of filter elements and ionizers in air handling units;

[0044] Fig. 19 is an isometric view illustrating an arrangement of a typical housing for an embodiment of the present invention; and

[0045] Fig. 20 is a diametric view of an alternative configuration of an embodiment constructed according to the principles of the present invention with parallel pleats and curved

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apexes; and

[0046] Fig. 21 is a diametric view of an alternative configuration of an embodiment constructed according to the principles of the present invention, with curved apexes.

DETAILED DESCRIPTION OF THE INVENTION

[0047] Turn now to the drawings collectively, and particularly to Fig. 1a, which shows an elevation view of an inlet side of a filter assembly 31 for an ionizing field electronically enhanced filter 100 with the ionizer assembly removed, Fig. 1b which shows enlarged details of the downstream outlet side of filter 100, and Fig. 1c which shows an elevation view of the downstream outlet side of filter 100. Filter 100 may be constructed with an exterior frame 24, that may be made of sheet metal, enclosing an array formed by one, or more, deep accordion folds of a pleated filter medium 1 covered, on the upstream, or inlet side, by the honeycomb pattern of a charge transfer electrode 5. It should be noted that only the outer portion of the lower arm of each pair of arms forming each pocket of filter medium 16 into a V-shaped pleat 52 of the composite filter medium 16 and transfer electrode 5. Filter medium 1 may be constructed with all of the several lower pleats all forming part of the same continuous layer of material 16, such as felt or alternatively, a mat.

[0048] End caps 2a, 2 extend horizontally across the inlet and outlet sides, respectively, between side frames 24. End caps 2a restrict the entrance of particulate bearing air, indicated by arrows "A", to the interstices remaining between end caps 2a, thereby forcing the air into one of the V-shaped pleats 52. Pleats 52 may be joined at an apex 50. End caps 2 on the outlet side

also restricts passage of the air to the V-shaped pleats. Consequently, particulate laden air drawn into the inlet side of filter 100, passes through the broad planar areas provided by the several pleats of filter medium 1.

[0049] Charge transfer electrodes 5 may be formed on the exposed outer surfaces of the V-shaped pleats on the inlet side of medium 16, while downstream ground electrodes 4 may be formed on the exposed, opposite outer surfaces of the V-shaped pleats 52 on the outlet side illustrated by Figs. 1b, 1c. Electrodes 4, 5 may describe honeycomb grid patterns as shown in Figs. 1a-1c, or any of various screen or grid patterns that cover the opposite exposed parallel sides of medium 16, to each form a discrete, continuous electrode 4, 5 that may be maintained at a single, constant and uniform potential. Electrodes 4 and 5 are electronically isolated from one another so that they may be maintained at different electrical potentials during operation of filter 100, and are physically separated by the thickness d_3 of medium 16. The depth of each V-shaped pleat 52 is somewhat less than the width of frame 24, and is a function of the thickness d_3 of medium 16. It is contemplated that downstream electrode 4 will be maintained at a local ground potential, while charge transfer electrode 5 will be maintained at a potential that has a higher magnitude than downstream electrode 4. Electrode 4 may therefore, be electrically connected to the sidewalls formed by frames 24 and to end caps 2, but electrode 5 must be electrically isolated from electrically conducting end caps 2a and from the electrically conducting frames 24 by air gaps 6. As is explained subsequently herein in the detailed discussion that accompanies Figs. 4a through 15, an ionizer assembly 30 constructed with a plurality of parallel ionizing electrodes 8 maintained at a high voltage relative to the local ground, may be attached to the exposed flanges

that frame the inlet of filter assembly 31, to locate individual ones of ionizing electrodes separated by identical air gaps having identical constant distances, d_2, from a corresponding planar surface of charge transfer electrode 5. The consistency of the values of the resulting air gaps, d_2, allows an uniform voltage to be induced onto charge transfer electrode 5, thereby establishing an uniform electrostatic field that extends across the thickness d_3 of medium 16 between charge transfer electrode 5 and downstream ground electrode 4.

[0050] Referring now to Figs. 2 and 3, I have found that with embedded corrugated spacers, variations occurring in the induced field depends on the distance d_2 between electrodes 8 and the upstream corrugated spacers at a fixed applied potential to electrodes 8. When both the tolerances in media folds and aluminum spacers are taken into account, this can mean large variations in induced potentials and hence in collection field strength and therefore in filtration performance within various sections of the filter medium.

[0051] Now consider the variation in the upstream corrugated spacer alignment with respect to the downstream spacers. Fig. 2 shows two of the many variations in alignment that are possible. In one case the alignment of the peaks are off by approximately 45 degrees. This results in Min1 and Max1 distances d_3, between the upstream and the downstream spacers. In this case the performance will vary from media section to section since the collection field strength will be inversely proportional to d_3 (collection field strength = Vinduced / d_3). Now consider the case (which must be considered because this will occur often within the filter media folds) when the spacers are mis-aligned by about 180 degrees - *i.e.*, peaks will coincide or almost coincide as shown in bottom section of Fig. 2. In this case of Min2, d_3 is equal to the media thickness and at

Max2, d_3 is equal to twice the depth of the spacers. The maximum induced voltage on the upstream corrugated spacer electrode in their device can only be about 0.35 kilo-Volts in order to safely eliminate sparking through the media (thereby preventing damage to the media and avoiding a fire) towards the opposite corrugated electrode spacer (which is also within the pleat) at ground potential on the other side of the pleat at the point where the peaks are aligned. This corresponds to a collection field strength of about 17 kilo-Volts/inch, but only when the peaks of the upstream corrugated electrode are facing (see Fig. 2) the corrugated counter spacer electrode on the opposite side of the media. A collection field strength of about 12-15 kilo-Volts/inch, is desirable for effective collection of particles on the filter media. Consider now that for the Max d_3 section of the media, the collection field strength at the mid-point of the corrugations will be 0.35 kilo-Volts/0.52" = 0.67 kilo-Volts/inch, if 0.25" separator corrugations (which are the smallest size corrugations that are available) are used. This collection field strength 0.67 kilo-Volts/inch is negligible for efficient filtration of particles from the air stream. This means that this section of the filter will have very low enhancement of filtration efficiency. If deeper pleated spacers are used, this situation is worsened. Of course, it should be noted that all sorts of situations in between these two situations can exist. Essentially, this results in a non-uniform performance. Keeping in mind that filters are mostly rated by their weakest performing section, this structural configuration will not result in high enough filtration enhancement.

[0052] Turning now to the issue of whether the structural configuration embedded separators shown in Fig. 2 has an unnecessarily high likelihood for sparking, Fig. 3 shows the voltage induction on the upstream electrodes as a function of distance from a wire electrode. Keeping in

mind that the upstream electrode cannot be induced to a voltage higher than about 0.35 kilo-Volts, one can clearly see how daunting the task of maintaining such a precise gap between each and every one of the upstream electrodes and the inducing wire. In the structural configuration of Fig. 2, for sparking, the electrodes are simply placed, unsecured between the media folds, it is highly likely that some of the electrodes will be closer than the target distance d_2 by as much as 3/16 of an inch. This will result in higher surface potential on those upstream corrugated electrodes that are closer to the high voltage wire, resulting in corona discharge and sparking at points where the peaks of the upstream and downstream corrugations of the electrodes align as in Fig. 2. Sparking will cause burn holes in the filter media and possibly cause a fire if the sparking is continuous sparking. Cheney '736 suggests the use of existing, commercially available aluminum separators embedded in deep pleat filters. I have found that in tests that I have done on filters constructed with embedded electrically conducting separators, it was not possible to get an aluminum separator filter to function without sparking and at the same time achieve a significant improvement in filtration. Even if a close to ideal manufacturing method for making such filters was to be developed that was able to control the distance between corrugated electrodes and the high voltage wire so that no sparking occurred, the resulting embedded filter would still demonstrate significant variation in surface potential and, therefore, collection fields across different portions of the filter.

[0053] Since the filter medium used in embedded electrically conducting separators should be highly porous (*e.g.*, porosity > 95%) and the minimum distance, d_2 Low, between the high voltage wire and the downstream corrugated electrode is not significantly greater than the

distance, d_2 High, between the wire and the upstream corrugated electrode, there will be a considerable amount of leakage current towards the downstream corrugated electrode which is maintained at ground potential. Any leakage current will make the device inefficient. This situation is worsened when the glass filter paper absorbs moisture as a result of high humidity.

[0054] In order to prevent sparking towards the frame material, the frame material in the practice of Cheney '736 must be non-conductive because the aluminum spacers of the upstream corrugated electrodes will have a high probability of contacting the frame material. Typically, wood products are used. Most current manufacturing methods have switched to the use of aluminum or metal channel frames since these are non-particle shedding, result in better seals to the media, and are not flammable. Cheney '736's wood is rather dirty for cleanroom applications.

[0055] It should be noted that Cheney '736 does not describe any electrode gap values or ranges of voltages used in any of the configurations, nor does it provide any results showing the efficacy of the embodiments disclosed. It is highly likely that these practical difficulties and performance limitations of the Cheney and Spurgin is the main reason why such a device has never been commercialized. Additionally, aluminum separator folded filter type filter elements have become unpopular because these filters tend to tear due to the sharp aluminum separators within the folded media operation.

[0056] Figs. 4 and 5 schematically illustrate several features implementing the principles of the present invention as two possible configurations of an ion izing, electrically enhanced filter modified according to the principles of the present invention with generally non-conductive filter media. A charge transfer conductive, perforated electrode 5 formed as a continuous grid is

placed upon and borne by the upstream surface of filter medium 1; electrode 5 is in complete electrical isolation from ground and from any counter potential electrodes 4, 7. I have found that tests show that the surface potential achieved on charge transfer electrode 5 with the embodiment shown in Fig. 4 is the same as the surface potential on the peaks of the filter medium charge transfer electrode 5 in the absence of electrically conductive, perforated electrode 5, which is the same result obtained in Jaisinghani U.S. Patent No. 5,403,383. The results are summarized below in Table I:

<Table I>

Configuration	Applied Voltage on Wires kilo-Volts	Surface Potential due to Charge Transport, kilo-Volts	Electrically Enhanced Filter Efficiency of 95% Media
Without CTE (5,403,383)	17	10.9	99.99%
With CTE	17	10.8	99.99%

[0057] Basically, these results clearly establish that in the "flat" configurations illustrated by Fig. 4, the addition of charge transfer electrode 5 neither aids nor affects the operation or performance of the EEF in any significantly manner.

[0058] Turning now to Fig. 5, if filter element 1 and charge transfer electrode 5 are both tilted at an angle, and another filter medium pack is added to form a V-shape, then the embodiment of this invention shown by Figs. 6 and 8 result. In this embodiment, the distance between ionizing

electrodes 8 and the control electrode 7, d_1, primarily determines the particle charging field strength, that is, the corona generation, which results in ion formation and charging of incoming particles carried by air entering filter 1 in the direction of arrow A.

[0059] The invention differs in the manner the particle collection field strength across the filter medium is established. In Jaisinghani U.S. Patent No. 5,403,383 the upstream plane of the filter medium achieves a uniform charge since the distance between the ionizing wires and the upstream plane of the filter is uniform. In this invention, since the filter medium is an a V pack formation, the closest portion of the filter medium would have the highest influx of charge while the furthest section would have the lowest or negligible amount of charge. In order to overcome this difficulty the charge transfer electrodes 5 (*i.e.*, CTE's 5) are utilized - the discharge of ions around the ionizing electrodes 8 is collected on the electrically conductive CTE 5, primarily at the portion of CTE 5 closest to ionizing electrodes 8. CTE 5 being electrically conductive, therefore achieves a constant potential across the upstream face of the V-pack filter media.

[0060] The mechanism involved is not simple electrical induction. Referring to Table II and Fig. 3, the charge is transferred well into the exponential or corona generation portion of the curve. Unlike the Cheney and Spurgin, the resulting potential on CTE 5 is at least an order of magnitude (actually two orders of magnitude in the example shown in Table II) higher than the estimated potential that could safely be induced on the separators of the Cheney and Spurgin reference. The charge is eventually transferred across the filter to the downstream ground electrodes via the small, but finite conductivity of the generally non-conductive and dielectric filter medium. There is a net equilibrium charge accumulated however, and this results in a high

surface potential, with a magnitude that is in between that of the applied voltage to the ionizing electrodes and the potential of the downstream ground electrodes, that are typically at ground potential. CTE 5 may be made of a conductive material such as aluminum or other metal, so that the potential is constant across the entire face of CTE 5. Thus the distance, d_2, controls the value of the CTE potential for any given applied potential on the charging corona wires. Since the downstream ground electrodes and the CTE 5 are essentially parallel because they run along the planes of the filter media, the collection field strength (V_{CTE} / d_3) is high enough when compared to that of the flat configurations of contemporary design and also stable and constant across the filter medium, and without risk of spark discharge across filter medium 1.

[0061] The charging device, or ionizer assembly 31, significantly ameliorates the cancellation of the ionizing field (V_{app} / d_1) caused by the capture of highly resistive dust on the upstream control electrode. In the practice of this invention, the particles of dust would have to travel against the direction of the airflow of transient air through interstices 190 in order to accumulate on control ground electrode 7. In many contemporary designs however, the electrodes are parallel to the path of air flow. Consequently, the dust particles that enter the system are close to the plates and are more easily captured on the plates. The resulting accumulation of these dust particles often causes field cancellation and back corona discharge in contemporary devices

[0062] Fig. 6 illustrates a deep V-pack arrangement of filter medium 16 arranged in a pleated configuration. This electrode configuration enables use of deep filter medium 16 in a safe, efficient and risk free manner - something that is not possible with contemporary designs. In this V-pack arrangement, the layer of filter medium 16 has numerous folds and undulates alternately

between the plane of downstream electrode 4 and upstream electrode 5. The extreme ratio between the length of each fold of medium 16 within the V-pack to the fineness of the pitch between successive folds enables the V-pack to contain much more filter media while providing a lower pressure drop along the path of the transient air flow.

[0063] A set of CTEs 5 are located on the upstream face of filter medium 16 and spaced apart by a distance d_2; in order that the potential difference between CTEs 5 and downstream ground electrode 4 is controlled principally by the potential difference between ionizing electrodes 9 and the local ground potential, contract transfer electrodes 5 should have no electrical contract with any other electrically conducting member. If the upstream end caps 2a that hold the V-packs in place are metal, then a gap 6, of about 0.25" is maintained between the end caps 2a and charge transfer electrode 5. On the downstream side, a set of perforated downstream ground electrodes (DGE) 4, are applied to filter medium 16. In this case it is actually preferred that the downstream end caps 2 be made of metal and that the downstream ground electrodes be in direct electrical contact with metal end caps 2. An electrical charge is transferred to CTEs 5 by ionizer assembly 30. Ionizer assembly 30 is a frame that is positioned spaced-apart from opposite pleats of medium 16, so as to hold ionizing electrodes 8 parallel to and spaced apart by a constant, fixed distance d_2 from V-pack filter assembly 31.

[0064] Referring again to Fig. 6, the gap d_2 between high voltage ionizing electrodes 8, and CTE 5, is such that the field strength across the filter medium 16, (defined as CTE potential divided by the distance d_3 between CTE 5 and the downstream ground electrode (DGE) 4), is essentially the same as the field strength across filter medium 16. Additionally, the gap d_1

between the high voltage ionizing electrodes 8, and the control electrode 7, is such that charging of airborne particles within transient air is achieved - *i.e.*, the charging field strength (defined as the potential applied to electrodes 8 divided by d_1) is similar to the field strength used in Jaisinghani U.S. Patent No. 5,403,383.

[0065] In the basic mechanism of filtration enhancement, ionizing electrodes 8 are positioned within charging range d_2 of charge transfer electrodes 5, and charge transfer electrodes 5 become electrically charged by ion flow from the corona of ionizing electrodes 8. Downstream ground electrode 4 is maintained at a local ground potential; consequently an electrical field is established across filter medium 16, between charge transfer electrode 5 and downstream ground electrode 4. The incoming particles are charged by the first ionizing field, V_{app}/d_1, and some of the bacteria entering may be killed in this zone. Ionizing electrodes 8 transfer charge to the CTEs 5, and thus an adequate and safe, non sparking collection field, V_{CTE}/d_3, is easily achieved across filter medium 16. Typical filter media 16 are manufactured by Camfill-Farr under their Filtra 2000 series, or are available from Airgard Corporation.

[0066] The operation of filter assembly 31 is a reduction in the penetration of particles across filter medium 16 by about two to three orders of magnitude, lower resistance to the flow rate of transient air (as compared to conventional or mechanical filtration) and an increase in filter life by about a factor of between about two to three. The increase in the filter's life is due to filter assembly 31 exhibiting a lower pressure drop and the formation of dendrites caused by the electrical field results in a higher porosity formation of dust layers on filter medium 16, which preserves the lower pressure drop across filter assembly 31.

[0067] The configuration using a V-pack filter assembly 31 illustrated by Fig. 6 may be compared to an embodiment of Jaisinghani U.S. Patent No. 5,403,383 in Table II. Embodiments of Jaisinghani '383 conveniently serves as a benchmark of electrical enhancement of particle removal efficiency, albeit with the concomitant deficiencies in the embodiment of Jaisinghani '383 noted in Table II.

<Table II>

Parameter	5,403,383	Deep V-pack w/ CTE
Vapp, kilo-Volts	17	12.5
d_1, inches	1.45	1.0625
Ionizing Field Strength, kilo-Volts/in	11.72	11.76
d_2 min dist from wire to media or CTE, inches	0.625	0.5625-0.625
Media peak or CTE surface potential, kilo-Volts	10.9	5.72
Media depth d_3, inches	2	1 - 11.5" deep V-pack
Collection field strength	5.45	5.72
Filtration Efficiency @ 0.3 micrometers @ 300 fpm, %	99.97-99.99	99.99
Filter Pressure drop @ 300 fpm face velocity	0.85" WC	0.25" WC
Filtration Efficiency @ 0.3 micrometers @ 600 fpm, %	99.93	99.97
Filter Pressure drop @ 600 fpm face velocity	1.75" WC	0.5" WC

In both cases the filter medium used has a non-enhanced filtration efficiency of between approximately 92-95% with entrapping airborne particles that are 0.3 micrometers in diameter.

[0068] Fig. 3 illustrates how the CTE potential in a deep V-pack configuration is determined

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by the distance d_2 between the ionizing electrodes 8, and CTEs 5, for any one particular set of values for V_{app} (the voltage applied to electrodes 8) and d_1. Fig. 16 on the other hand shows how the magnitude of the potential across CTE 5 and DGE 4 increases as a function of the amplitude of the voltage applied to electrodes 8, for constant values of d_2 and d_1. As illustrated by Fig. 17, there is a region where V_{CTE} is very low and linear with respect to V_{app}. Once the V_{app} is greater in magnitude tha n the corona onset voltage (the corona onset voltage depends also on d_1) however, then the value of V_{CTE} increases exponentially with respect to V_{app}. This indicates that the charge transfer mechanism between ionizing electrodes 8 and charge transfer electrodes 5 is charge transport rather than simple electrical induction.

[0069] The embodiment illustrated by Fig. 6 attains higher performance at higher flow rates with lower pressure drop or flow restriction as compared to both conventional filters and embodiments of Jaisinghani U.S. Patent No. 5,403,383.

[0070] Two other configurations are shown by Figs. 8 and 9. In Fig. 8 CTE 5 is held against the upstream face of thick, non-pleated filter medium 16. This is one distinction between the embodiment illustrated by Fig. 8 and the configuration of Fig. 6. It is important to note that in these configurations CTE 5 is made of flat metal plates perforated by numerous interstices 160 accommodating passage of transient air, with every part of CTE 5 positioned essentially in direct physical contract with the upstream outer exposed, major surface of filter medium 16; CTE 5 does not function as a spacer and hence need not be in corrugated form as the aluminum spacers used in the contemporary designs represented by Cheney *et al.* U.S. Patent No. 4,781,736. As discussed previously, with spacers that are corrugated, the field strength across the filter medium

is non-uniform and can result in sparking and the burning of holes in and through the filter medium.

[0071] Fig. 8 shows the deeper, non-pleated medium 16. An example of this would be the use of flat, continuous fiber glass mats or felt of polymeric materials lying between essentially parallel electrodes 5, 4 in non-pleated form as a linear continuum extending between end-caps 2, 2a over the length of each pleat. In this configuration, although end caps 2, 2a are shown, it is not necessary for end caps to be used. Medium 16 can simply be folded at each end of a pleat as shown in the case of the relatively thinner thickness d_3 of paper medium 17 illustrated by Fig. 9. If flat, continuous mats are used in each pleat of the construction of the Fig. 8 embodiment however, CTE electrodes 5 must be shorter than each pleat of filter medium 5 by approximately, 0.25" to 0.06", depending on the design CTE voltage, as is shown by Fig. 9.

[0072] Fig. 9 shows the configuration using non-pleated, folded, thin paper medium 17. When filter medium 17 is in a very thin paper form, even when in the non-corrugated spacer electrode configuration shown, it can become extremely difficult to assure that no sparking or electrical discharge occurs anywhere across the structure of medium 17. In that case, a small air gap between CTE 5 and filter medium 17 may be maintained so as to enable sta ble and safe operation. The gap 18 may be maintained with spaces 180 made of a relatively lower electrical resistance glue beads, although other higher resistance polymeric spacers may also be used. The addition of gap 18 enables the device to operate at a higher and more stable potential difference between CTE5 and ionizing electrodes 8. Effectively, the distance d_3 is increased by the non-electrically conducting, insulators 180 serving as spacers between CTE 5 and the upstream outer

surface of medium 17, and this compensates for the higher, and more stable CTE potential which is controlled by distance d_2 and the ionizing field strength V_{app}/d_1. This assures proper and stable collection field strength for operation without arcing. CTE electrodes 5 must be shorter than the pleats in filter medium 17 by approximately, 0.25" to 0.06", depending on the design CTE voltage.

Printed Conductive CTE (Fig. 5d)

[0073] Turning now to Figs. 10 and 11, CTE 5 is deposited as an electrically conductive pattern 5 that may be printed directly onto the upstream outer surface of filter 16 in a grid such as a honeycomb pattern, by using a conductive ink or paint with appropriate openings to simulate a perforated electrode. Conventional photolithographic or stamping techniques may be used to create such a pattern on the upstream surface of filter medium 16. In this case there is no necessity of using metal plates for CTE 5, although plates of an electrically conductive material could be used if the pleated configuration was used with CTE 5 deposited on the upstream surface of filter medium 16 and if the conductivity of the printed CTE 5 was not high or had an intermediate level. In that case, the printing will enable a higher collection field strength without the application of a higher amplitude of V_{CTE} or without reducing the value of d_2 to an untenably low value. All other aspects of this embodiment may be constructed similarly to those illustrated by Figs 6, 8 and 9.

[0074] A dual filter layer configuration is illustrated by Fig. 12 and may be constructed according to the principles of the present invention, with an electrically conductive fibrous layer 19 which serves as a pre-filter, or a porous paper layer 19 may be used, instead of the electrically

conductive metal CTE 5, on the upstream exterior surface of the non-electrically conductive filter medium 17. This conductive fiber configuration can also function as a pre-filtration device. Although Figs 12 only shows a dual media 19, 17 with the flat filter medium 17 configuration, it should be noted that this method can also be applied to the pleated configuration of medium 16 illustrated by Fig. 6. It should be noted that when using dual media 19, 17 configuration, it is important that a small gap 6 of between approximately 0.04 to about 0.25 inches be maintained between control ground electrode 7 and conductive medium 19 which functions as the CTE charge transfer electrode.

[0075] Turning now to Fig. 13, resistive control of transfer electrode 5 may be established in order to maintain CTE 5 at a potential other than the local reference, or ground potential. Instead of letting CTE 5 float or be totally electrically isolated, CTE 5 may be connected to a local reference potential such as a ground or to the opposite downstream ground electrode 4 via a high resistance resistor R_{20} in the mega-ohm range. Resistor R_{20} is coupled in parallel to the much higher resistance of filter medium 16, 17. This will limit the accumulated charge on CTE 5, resulting in a lower or limiting potential at CTE 5. Thus, technique may be used to control the CTE potential in addition to varying the distance d_2. This technique may be useful when d_2 is small and slight and precise variations of d_2 are not practical. The use of resistor R_{20} provides a secondary way of controlling the collection field strength and also ensuring the safety of filter device 1 by inhibiting arcing. Fig. 13 shows resistor R_{20} applied to the configuration detailed in Fig. 6. This technique may be used in one or more of the several possible combinations with the other basic configurations described here using either flat or deeply pleated V-packs.

[0076] Referring now to Fig. 14, the ionizer is constructed to provide separate ionizer and charge transfer fields. In the embodiments illustrated by Figs. 6, 8, 9, 10 and 12, the ionizer electrodes 8 serve to both ionize the incoming gas or air based on V_{app} and d_1 and to transfer the charge to the CTE 5, in dependence on d_2. In order to separately control ionization, the charging of airborne particles and the charge transfer to the CTEs 5, a separate set of electrodes 184 on longer ceramic standoffs 13 with ionizing electrodes 8 linearly spaced-apart from particle ionizing electrodes 184 may be used. The shorter standoffs are used to suspend ionizing electrodes 184 for the particle charging field. Alternatively, a totally separate ionizer may be used and a totally separate charge transfer set of electrodes 8 may be used with separate high voltage connections to particle charging electrodes 184 and ionizing electrodes 8. In this latter configuration, it may be necessary to use two different high voltage power supplies, depending on the actual design.

[0077] Referring now to Figs. 1, 6, 15, 17, 18 and 19 collectively, the configurations described in the foregoing paragraphs may be put into practice with either deep V-pack pleated filters made with glue beads, ribbon separators or a separatorless mini-pleated filter medium 16 illustrated in Fig. 6, or with an unpleated, continuously flat filter medium 17, regardless of whether the filter medium is constructed with thick felt of fiber mat or with in a thinner layer made of a porous material such as paper, as is shown by Figs 8 and 9.

[0078] Within each of these embodiments it is understood that variations such as the printed CTE 5 as shown in Fig. 11, resistive control of CTE potential as shown in Fig. 13, dual relatively conductive media CTE as shown in Fig. 12 and alternate ionizer with separate CTE charging as

shown in Fig. 14, may be incorporated, in different variations.

[0079] Figs 1a, 6, and 15 show a typical V-pack filter constructed by using filter medium packs 1, or approximately 1" deep glue bead or ribbon separator filter medium mini-pleats or separator-less mini-pleats arranged in a multiply pleated, deep V formation so that individual neighboring pairs of the pleats form the apex of the V within a downstream end-cap 2. The packs are typically sealed within the end cap using a polymeric flexible adhesive 3 such as urethane plastisol. The transverse surface of the packs and the ends of the end-caps are sealed to the filter frame 24 by potting the packs and the end-caps to the frame of the V-pack using similar adhesives. The frame of the filter is typically made using aluminum or galvanized channels and clips 27 which hold it together. The insides are potted with a urethane or other similar adhesive to form a solid frame that is sealed to prevent detectable leakage.

[0080] End caps 2 shown by Fig. 1b on the downstream side of the filter are preferably made of an electrically conductive metal, which is in electrical continuity with the metal framing material or channel that encompasses the filter as a housing. The downstream ground electrode plates 4 are inserted within end caps 2 in electrical contact to provide electrical continuity with end caps 2and hence the frame of the filter. Thus, only one point on the frame of the filter needs to be grounded or set to a opposing potential in order that all of t he downstream ground electrodes plates 4 will be at the same potential. This grounding may typically accomplished by a metal grounding clip 47, which contacts the filter end caps as the filter is tightened against the seal plate 34 as shown by Fig. 19. Different mechanical devices that enable ground contact may also be used in lieu of grounding clip 47.

[0081] End caps 2a on the upstream side as shown by Fig. 1a are preferable made of a non-conductive material or plastic extrusion. In this case, CTE plates 5 can then be maintained securely within upstream plastic end caps 2a, and gap 6 shown in Figs. 1a, 6 and 8 is not then required. Thus, since the entire inside of the V-pack is potted with a non-conductive plastisol, the CTE plates 5 are essentially maintained in electrical isolation. It is, however, not essential that upstream end caps 2a be made of a non-conductive material. It is possible to use metal end caps as in the downstream end caps, provided that CTE plates 5 are not in electrical contact with elements of filter 31 that are at a different potential, and gap 6 is maintained with these metal end caps 2a shown by Fig. 1a and Fig. 6. Typically, a separation distance of about 0.375", thatis, gap 6, is maintained between CTE plates 5 and metal end caps 2a to ensure that there is no electrical discharge and proper isolation of CTE plates 5. This, then enables easy conversion of a manufacturing process that is already set up to manufacture conventional V-pack filter elements with metal end caps only.

[0082] The non-pleated filter medium 17 may be incorporated into a non-pleated configuration suitable for use in lower efficiency filtration applications, although non-pleated filter media may be adapted to higher filtration applications also. The filter medium may be in a flat, continuous thick mat or felt form 16 as shown in Fig. 8, or in thin paper form 17 as shown in Fig. 9.

[0083] Fig. 17 shows two embodiments of the filter 186, 188 with filter medium 16, 17 bonded into the preferably non-electrically conductive frame of filter assembly 24 to form a potted filter element 186 via a plastisol or other adhesive as in the case of the V-pack filter described above, with filter medium 16, 17 maintained in direct contact via light bonding by

means of an adhesive to downstream ground electrodes 4 which is in an electrically conductive, continuous, deeply pleated and perforated form. CTE 5 may similarly be a continuous pleated and perforated, electrically conductive member that is also bonded to the non-electrically conductive frame. If the filter medium is very thin paper, depending on the electrical design, a small gap 18 of about 0.04" to 0.25" may be maintained between CTE 5 and the upstream surface of filter medium 17 in order to achieve charge stability without risk of spark discharge. Glue beads 180 may be used to also ensure this separation distance 18. This embodiment is a throw-away filter and is deployed for high filtration efficiency applications.

[0084] Fig. 17 shows the non-pleated media 17 embodiment 188 which enables a user to simply replace the filter media when it gets dirty, rather than throwing away the entire filter assembly. Consequently this embodiment is usually not deployed for high filtration efficiency where high filtration efficiency is defined as (greater than 95% at sub-micron particle sizes) applications. Non-conductive frame 24 which may be part of a fan-filter housing or may be a separate component within such a housing, is used. CTE 5 is attached to this frame and is in a continuous pleated and perforated conductive form. Downstream ground electrodes 4 which is also a continuously pleated and perforated, electrically conductive member, is removable and is designed to fit into the pleated form of CTE 5 , which is constructed as a discrete member, such that there is enough room for filter medium 17 in between CTE 5 and electrode 4 when the downstream ground electrode 4 is attached to the frame via a set of screws 41 or other fasteners such as clips. Downstream ground electrode 4 has a flanged edge 39 which is sealed against the edge flange of filter frame 24. The edge of the filter medium 16, 17 is sealed to the frame by a

layer of fiberglass or mat 40 or another material, that is able to prevent the passage of dust, that is glued to the top inner and bottom surfaces of filter frame 24. Alternatively, the system can be designed such that CTE 5 is removable and the downstream ground electrode 4 is fixed into the filter frame. Other techniques may also be used to enable filter media replacement in the practice of this invention.

[0085] If a very thin filter medium 17 is to be used, then CTE 5 and downstream ground electrode 4 may be fitted with fastening points to the frame 24 so that there is there is space between the CTE 5 and electrode 4 for the media plus about 0.04"-0.25", depending on the design of CTE 5 and the voltage applied to CTE 5. Typically the filter medium used is attached to the downstream ground electrode 4 member by means of either Velcro® strips attached to various points on the downstream ground electrodes and on corresponding points on the filter medium. Filter medium 17 is usually manufactured with folds or creases, which coincide with the pleats of downstream ground electrode 4 to facilitate attachment of the filter medium to downstream ground electrode 4. To replace filter medium 17, the downstream ground electrodes 4 is detached from the frame 24 and the dirty filter medium is replaced with a clean new folded medium.

[0086] Figure 15 is a blown up view of ionizer 30 and filter assembly 31 illustrating how ionizer 30 is used in conjunction with deep V-pack filter assembly 31. It should be noted however, that ionizer assembly 30 is mounted to either of the above filter embodiments in the same manner in order to create a working electrically enhanced filter configuration. Hence, the ionizer 30 is also applicable to the non-pleated filter embodiment.

[0087] The ionizer assembly 30 shown in the enlarged view in Fig. 6 in constructed with a perforated metal plate 7, with or without the pre-filter channel 25 or other mechanism used to hold a prefilter at the upstream face of the ionizer. Onto this plate 7 high voltage electrodes 8, typically made of Tungsten are mounted at a separation of distance d_1 from the perforated metal plate. Electrodes 8 are mounted in pairs or sets of wires, spaced between 0.75"-1.5"apart, onto a bus bar 10 which is in turn mounted on top of dielectric and non-electrically conductive standoffs 13 made of non-electrically conducting material such as a ceramic. Stand-offs 13 typically are threaded on the inside at both ends so as to enable mounting via screws 12 on to perforated metal plate 7 on one end, and the conductive metal bus bar 10 on the other end of each standoff 13. Electrodes 8 are then attached typically via springs 9 to holes 15 by using loops on the spring, to bus bars 10. High voltage is applied to bus bar 10 and thence to electrodes 8 via high voltage cable 11 which is typically connected to a high DC voltage power supply via quick connect high voltage couplers.

[0088] In order to eliminate any potential arcing from any rough metal surface of the ionizer's 30 bus bar 10, springs 9 or wire or spring loops, a dielectric non-electrically conductive C-shaped, channel shield 14 may be used to shield these components from other surfaces as shown in the enlargement of Fig. 6. Alternatively, instead of a C-channel, a flat dielectric plate covering the top of the entirety bus bar 10 and spring assembly may be used. Typically, non-electrically conducting materials such as acrylic or appropriate nylon, which have high electric arc track resistance, may be used to form shield 14.

[0089] Referring to now Fig. 15, ionizer assembly 30 may be attached to filter assembly 31

using fasteners such as threaded bolts or screws 23 which fit into metal guide tabs 21 attached to the exterior of filter housing 24. A wing nut 22 or other removably receptive fastener may be used to secure bolts 23. Tabs 21 enable sets or pairs of ionizer electrodes 8 to be correctly spaced within each V-shaped pair of pleats of filter assembly 31, while maintaining correct values of d_2 (cf Table II). The maintenance of proper values of d_2 for each set of ionizing electrodes 184 and charge transfer electrodes 8 is important to assure the safe and efficient operation of the deep electrically enhanced filter.

[0090] Fig. 18 shows a housing that can be used to mount single or multiples of such filters and ionizers in air handling units 38. A filter frame assembly 32, which is sealed against a seal plate 34 in air handling unit 38 either by welding or other means such as by using polymeric seal materials. Frame assembly 32 has members 29 mounted on each of the four sides; members 29 are formed from brackets with holes onto which a L-shaped rod with threaded bolt on the end are inserted. At the threaded end is a L-shaped washer with a nut that threads on to the L-shaped rod. This and other such filter sealing assemblies are available from companies such as Camfil-Farr and AirGard among many others, and hence this mechanism need not be drawn in detail or described further here.

[0091] Filter assembly 31 and ionizer assembly 30 are first assembled together and then inserted into frame 32, as an united assembly, and then the nuts and L washers or clips on sealing member 29 are tightened to be pulled over the edge of ionizer control electrode 8, which pulls the entire assembly together, thereby compressing gasket 26 against sealing surface 34.

[0092] In the assembly shown by Fig. 18, it is not possible to use metal guide tabs 21, as

shown in Fig. 15, because there is typically no room for guide tabs 21 on the side of filter frame assembly 32. In this case, ionizer assembly 30 is accurately guided into filter assembly 31 by a set of four channel guide members 33. Ionizer assembly 30 rests snugly inside the space created by guide members 33. Sealing member 29 then holds assemblies 30 and 31 together.

[0093] Figs. 18 and 19 show housing 38 along with the connections of air inlet 42 and outlet duct 43. Housing 38 typically contains a fan 35, cooling and heating coils (not shown) and the filtration system of ionizer 30 and filter assembly 31. Fig. 19 also shows electrical box 37, which is mounted on the outside of air handler housing 38. This box contains the high voltage power supplies, indicator lights, switches and controls that enable control the filtration system. Housing 38 also has a service door, which is typically a walk-in door to change the multiple number of filters. For single filters, the service door is located so that the filter seal member 29 and the threaded fasteners are easily accessible from the outside.

[0094] Fig. 19 shows an isometric view of a typical housing 44 that is separate from the air handling housing 38, that can be used within a duct system that is connected to air handling unit housing 38. The typical housing 44, often referred to as an in-duct filter housing, uses of an optional fan 35 when the central air handling unit fan does not have enough power to draw the air through the enhanced filter system, electrical component compartment 37, seal plate 34 and service door 36. The controls and indicators 46, are mounted on the outer surface of electrical compartment 37. A grounding clip 47 of an electrically conducting material such as metal, forms an electrical path of conduction between downstream ground electrode 5 via end cap 2, and the electrically conducting frame of filter assembly 31. The frame of filter assembly 31 serves as a

local reference potential such as ground, and may be electrically coupled to a ground potential, such as earth, with a grounding strap (not shown). Filter 30 and ionizer 31 assemblies are also shown without detail. If fan 35 is not required in the construction of a particular embodiment, a flow switch may be used so that when there is no airflow, then the high voltage power supply to the ionizer wires is shut down. Service door 36 is positioned so that when door 36 is open, a safety disconnect switch is opened so that all power to the filter unit is disconnected.

[0095] The downstream side the filter has a polymeric (typically closed cell polyurethane foam or rubber) gasket 26 with sufficient hardness for sealing assembly 31 against seal plate 34. Filter assembly 31 is then sealed against seal plate 34 by either applying external force against ionizer assembly 30 by incorporating a bracket 48, which is threaded to move a bolt 49 with knob attached as is shown by Fig. 19, or by tightening nuts or wing nuts 22 onto bolts that are attached to the seal plate. These bolts can also go through the metal guide tabs 21 that are welded on to filter assembly 30. Alternatively, placement of sealing member 29 onto filter frame 32, enables attachment of springs that pull filter assembly 31 onto the seal plate as shown by Fig. 18. Only the sealing configuration is shown in Fig. 19. Filter assembly 31 can also be sealed against seal plate 34 by a variety of other common and conventional sealing mechanisms. The sealing mechanism is not shown in detail in Fig. 19.

[0096] Fig. 20 illustrates the construction of an alternative embodiment with at least one of the pockets in the filter assembly 31 formed by a pair of pleats 52 line in substantially, approximate parallel planes joined at the downstream, closed and by a curved, or C-shaped, apex 50, rather than a V-shaped apex. The ionizing assembly 30 may be constructed with a single electrode 8,

rather than an array formed by a plurality of electrodes 8, spaced approximately equidistantly between the upstream surfaces of CTE 5 of each pleat 52. Ceramic spacers 18, such as glued beads, may be used to electrically separate CTE 5 from the unfolded, thinner medium 17.

[0097] Fig. 21 illustrates the construction of an alternative embodiment with potentially intersecting pleats 52 joined at a curve, or C-shaped apex 50. Ionizing assembly 30 may be constructed with a pair of ionizing electrodes 8, each separated by a least distance d_2 from the closest surface of CTE 5.

[0098] The foregoing paragraphs describe the details of a method and apparatus that uses deep filters as an efficient and safe electrically enhanced filter (EEF) in order to obtain ultra low pressure drop, high efficiency of particulate removal and high dirt holding capacity and life of the filter. The EEF is constructed with a housing (with or without an internal air moving device such as a fan), and a deeply pleated filter preferably a V-pack filter with sets of downstream ground electrodes 4 and charge transfer electrodes 5 borne by the opposite, major parallel outer surfaces of filter medium 16, 17 assembled in a filter pack within as a unified filter element. Seal plate 34 seals the gasket on the filter element against an ionizer assembly to prevent blow-by of air; ionizer assembly 30 ionizes the gas and charges particles entering between the deep pleats of the filter element and also transfers a charge to the charge transfer electrodes 5 on the filter pack. A high electrical potential is applied to electrodes 8 or other charging elements in the ionizer and in some cases a fan 35 or motor assembly. Charge transfer electrodes 5 enable the device to function with a high particle collection field between charge transfer electrodes 5 and downstream grounded electrodes 4 that enables higher entrapment of the particles on the filter

medium, in a safe and efficient manner. In effect, the use of the charge transfer electrodes (CTEs) 5 allow the deeply pleated filter to function as a filter while avoiding the inherent inability of contemporary designs for filters to accommodate a greater depth of the filter element.

[0099] Ionizer assembly 30 has a control ground electrode 7 and high voltage electrodes 8 with appropriate shielding. This configuration stabilizes the corona and minimizes the possibility of field cancellation or back corona discharge as a result of coating of counter electrode 7 with highly resistive dust. The high field strength between control ground electrode 7 and the high voltage applied to electrodes 8 results in corona charging of incoming airborne particles. In the practice of this invention, the distances between the control ground electrode 7 and electrodes 8, and the spacing between electrodes and the CTEs 5 determine the surface potential developed on CTE 5 and hence the collection field between CTEs 5 and the downstream ground electrodes 4. In alternative embodiments, control ground electrode (CGE) 5 and downstream ground electrode (DGE) 4 may be at either a negative or at a lower potential with respect to the applied potential, and do not need to be rather strictly at ground potential.

[0100] Additionally, although contemporary devices accumulate dust in patterns that can sometimes generate undesired back corona discharge, embodiments constructed according to the principles of the present invention require that the dust would have to travel against the direction of the air flow in order to accumulate on ground plate 7; this minimizes the risk of back corona discharge that has plagued contemporary filters due to accumulations of dust.

[0101] The foregoing discussion describes the details of a method and apparatus using deeply pleated filters to provide efficient and safe electrically enhanced filtering (EEF), with ultra low

pressure drop, higher efficiency of particulate removal and higher dirt holding capacity over the life of the filter. An EEF may be constructed with a housing, with or without an internal air moving device such as a fan, a deeply pleated filter, preferably a V-pack filter with sets of downstream ground electrodes and charge transfer electrodes borne by the exterior surface of the filter packs that form the filtering element. An ionizer assembly that ionizes the gas and charges particles entering the deeply pleated filter and also transfers a charge to the charge transfer electrodes on the filter pack. A plate seals the gasket on the filtering element against the ionizing assembly. A high electrical potential is applied to charging elements in the ionizer and, in some embodiments, a fan or motor assembly. The charge transfer electrodes enable the device to function with a high particle collection field between the charge transfer electrodes and the downstream grounded electrodes to safely and efficiently attain higher entrapment of the particles on the filter medium.

What I claim is:

1. An electrically enhanced filtering apparatus, comprising:

a layer (16, 17) of a porous filter medium exhibiting a thickness, folded into one or more arms forming a pocket with an apex of said pocket located on a downstream side of said medium and with a base of said pocket open to an upstream side of said apparatus;

a first electrically conducting grid (4) disposed to cover said downstream side of each of said arms;

a second electrically conducting grid (5) electrically separated from said first grid by said thickness, disposed across each of said arms on an upstream side of said medium; and

an electrode (8) separated from said upstream side of said medium, with said electrode spaced-apart by a fixed distance from opposite corresponding ones of said arms while extending through said pocket parallel to and spaced-apart from said second grid.

2. The apparatus of claim 1, further comprised of said base exhibiting a linear dimension greater than said thickness.

3. The apparatus of claim 1, further comprised of a distance between said base and said apex being greater than or equal to a linear dimension exhibited by said base.

4. The apparatus of claim 1, further comprised of a distance between said base and

said apex being not less than a linear dimension exhibited by said base, and said linear dimension being greater than said thickness.

5. The apparatus of claim 1, further comprised of:

an air inlet; and

an electrically conducting screen spaced-apart from said electrode and spaced-apart from said second grid, extending across said air inlet.

6. The apparatus of claim 1, with said layer further comprised of:

said layer disposed in a plurality of pleats within each of said arms, with said pleats undulating toward between said first grid and said second grid.

7. The apparatus of claim 1, further comprised of:

said layer extending along each of said arms in a linear continuum lying between said first grid and said second grid.

8. The apparatus of claim 1, further comprised of said layer extending along each of said arms in a linear continuum lying between said first grid and said second grid.

9. The apparatus of claim 1, further comprised of:

said layer extending along each of said arms in a linear continuum lying between said first grid and said second grid; and

an electrical insulator maintaining said second grid physically spaced-apart from said medium.

10. The apparatus of claim 1, further comprised of:

said arms being joined at said apex to form a V-shape.

11. The apparatus of claim 1, further comprised of:

said arms being substantially parallel and being joined at said apex.

12. The apparatus of claim 1, further comprised of:

said second grid being borne by said upstream surface and lying upon said arms.

13. The apparatus of claim 6, further comprised of:

said second grid being borne by said upstream surface and lying upon said pleats.

14. The apparatus of claim 1, further comprised of:

an electrical insulator maintaining said second grid spaced apart from said upstream surface.

15. The apparatus of claim 1, further comprised of:

said second grid comprising a material porous to passage of gaseous fluid through said apparatus but partially impervious to particles borne by the gaseous fluid.

16. The apparatus of claim 1, further comprised of:

said second grid comprising a material porous to passage of gaseous fluid passing through said apparatus but partially impervious to particles borne by the gaseous fluid; and

said second grid being relatively more electrically conductive than said medium.

17. The apparatus of claim 1, further comprised of;

said second grid comprising a material porous to passage of gaseous fluid passing through said apparatus but partially impervious to particles borne by the gaseous fluid; and

said second grid being made of a material selected from a group comprising carbon, carbon fibers coated with carbon.

18. The apparatus of claim 1, further comprising at least one of said first grid and said second grid being made of a material selected from a group comprised of carbon, carbon fibers and fibers coated with carbon.

19. The apparatus of claim 1, further comprising:

a first electrical conductor coupling said first grid to a local reference potential;

a second electrical conductor disposed to couple said electrode to a second and substantially different potential; and

an electrical insulator maintaining said second grid at a first potential difference relative to said electrode, and at a second potential difference relative to said first grid.

20. The apparatus of claim 1, further comprising:

a first electrical conductor coupling said first grid and to a local reference potential;

a second electrical conductor disposed to couple said electrode to a second and substantially different potential.

21. The apparatus of claim 1, further comprising:

an inlet accommodating egress of gaseous fluid into said apparatus; and

an electrically conducting screen spaced-apart from said electrode and spaced-apart from said second grid, extending across said inlet and establishing a potential difference between said electrically conducting screen and said electrode that creates significant ionization of the gaseous fluid.

22. The apparatus of claim 1, further comprising:

a first electrical conductor coupling said first grid and to a local reference potential;

a second electrical conductor disposed to couple said electrode to a second and substantially different potential; and

an electrical insulator maintaining a first potential difference between said electrode and ① said local reference potential, with ② exhibiting a magnitude lower than said first potential difference, occurring between said second grid and said local reference potential.

23. The apparatus of claim 1, further comprising:

a first electrical conductor coupling said first grid and to a local reference potential;

a second electrical conductor disposed to couple said electrode to a second and substantially different potential;

an electrical insulator maintaining a first potential difference between said electrode ① a second potential difference ② an inlet accommodating egress of gaseous fluid into said apparatus; and

an electrically conducting screen spaced-apart from said electrode and spaced-apart. from said second grid, extending across said inlet and establishing a third potential difference between said electrically conducting screen and said electrode.

24. The apparatus of claim 1, further comprising:

a first electrical conductor coupling said first grid and to a local reference potential;

a second electrical conductor disposed to couple said electrode to a second and substantially different potential;

an electrical insulator maintaining a first potential difference between said electrode ① a second potential difference ②;

an inlet accommodating egress of gaseous fluid into said apparatus; and

an electrically conducting screen spaced-apart from said electrode and spaced-apart from said second grid, extending across said inlet and establishing a third potential difference between said electrically conducting screen and said electrode that creates significant ionization of the gaseous fluid.

25. An electrically enhanced filtering apparatus, comprising:

a layer of a porous filter medium (16, 17) exhibiting a thickness between a major upstream surface and a major downstream surface, folded into a pocket with one or more arms of pleats of said upstream surface extending in an upstream direction from an apex of said pocket toward an open base of said pocket;

a first electrically conducting grid (4) borne by said downstream surface and lying upon said arms;

a second electrically conducting grid (5) electrically separated from said first grid by said thickness, extending across said upstream surface of each of said pleats; and

a plurality of electrodes (8) spaced apart from said second grid (5) and positioned within said pocket between said apex and said base, extending along different corresponding ones of said arms in parallel alignment with said apex.

26. The apparatus of claim 25, further comprised of:

a first electrical conductor coupling said first grid to a local reference potential;

a second electrical conductor disposed to couple said electrodes to a second and substantially different potential; and

an electrical insulator interrupting direct electrical continuity between said first grid and said second grid.

27. The apparatus of claim 25, further comprised of:

an electrical insulator maintaining said second grid spaced apart from said upstream surface of each of said arms.

28. The apparatus of claim 25, further comprised of:

said second grid comprising a material porous to passage of transient air through said apparatus but impervious to particles borne by the transient gaseous fluid.

29. The apparatus of claim 25, further comprised of:

said open base exhibiting a linear dimension greater than said thickness.

30. The apparatus of claim 25, further comprised of:

a distance between said open base and said apex being greater than or equal to a linear dimension exhibited by said open house.

31. The apparatus of claim 25, further comprised of:

a distance between said open base and said apex being not less than a linear dimension exhibited by said open base, and said linear dimension being greater than said thickness.

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32. The apparatus of claim 25, further comprised of:

a channel forming an air inlet accommodating passage of the transient gaseous fluid; and

an electrically conducting screen spaced-apart from said plurality of electrodes and spaced-apart from said second grid, extending across said air inlet.

33. The apparatus of claim 25, further comprised of:

said layer along each of said arms in a plurality of folds undulating alternately between said first grid and said second grid.

34. The apparatus of claim 25, further comprised of:

said layer extending along each of said arms in a linear continuum positioned between said first grid and said second grid.

35. The apparatus of claim 25, further comprised of:

said layer extending along each of said arms in a linear continuum positioned between said first grid and said second grid; and

an electrical insulator preventing direct electrical continuity between said second grid and said medium while maintaining said second grid physically spaced apart from said layer.

36. An electrically enhanced filtering process, comprising:

positioning across a flow of transient gaseous fluid, a porous filter medium exhibiting a thickness and folded into one or more arms forming a pocket with a closed apex on a downstream sides of said medium and with a base of said pocket opening upstream sides of said arms to incidence of said flow;

maintaining a first electrically conductive grid borne disposed along said downstream sides of said arms able to accommodate passage of the transient air from said medium;

maintaining a second electrically conductive grid covering said upstream sides of said arms in a position spaced-apart from said first grid to accommodate said passage of the transient gaseous fluid, at a potential difference relative to said first grid; and

locating a first electrode within said pocket at a location within the flow of the transient gaseous fluid, spaced-apart from and parallel to said second grid, and disposed to transfer a charge onto said second grid.

37. The process of claim 36, further comprised of:

coupling said first grid to a reference potential; and

establishing said potential difference between said second grid and said first grid by applying to said electrode a potential difference relative to said reference potential.

38. The process of claim 36, further comprised of:

maintaining a control electrode spaced-apart and upstream from said first electrode, within the flow of the transient air.

39. The process of claim 36, further comprised of:

arranging said medium along each of said arms with a plurality of folds undulating alternately toward said first grid and said second grid.

40. The process of claim 36, further comprised of:

arranging said medium along each of said arms in a linear continuum positioned between said first grid and said second grid.

41. The process of claim 36, further comprised of:

extending said medium as a layer along each of said arms in a linear continuum positioned between said first grid and said second grid; and

electrically isolating said second grid from direct electrical continuity with said medium.

ABSTRACT

A method and apparatus using deep pleated filters to provide efficient and safe electrically enhanced filtering (EEF), with ultra low pressure drop, higher efficiency of particulate removal and higher dirt holding capacity over the life of the filter. An EEF may be constructed with a housing, with or without an internal air moving device such as a fan, a deeply pleated filter, preferably a V-pack filter with sets of downstream ground electrodes and charge transfer electrodes borne by the exterior surface of the filter packs that form the filtering element. An ionizer assembly that ionizes the gas and charges particles entering the deeply pleated filter and also transfers a charge to the charge transfer electrodes on the filter pack. A plate seals the gasket on the filtering element against the ionizing assembly. A high electrical potential is applied to charging elements in the ionizer and, in some embodiments, a fan or motor assembly. The charge transfer electrodes enable the device to function with a high particle collection field between the charge transfer electrodes and the downstream grounded electrodes to safely and efficiently attain higher entrapment of the particles on the filter medium.

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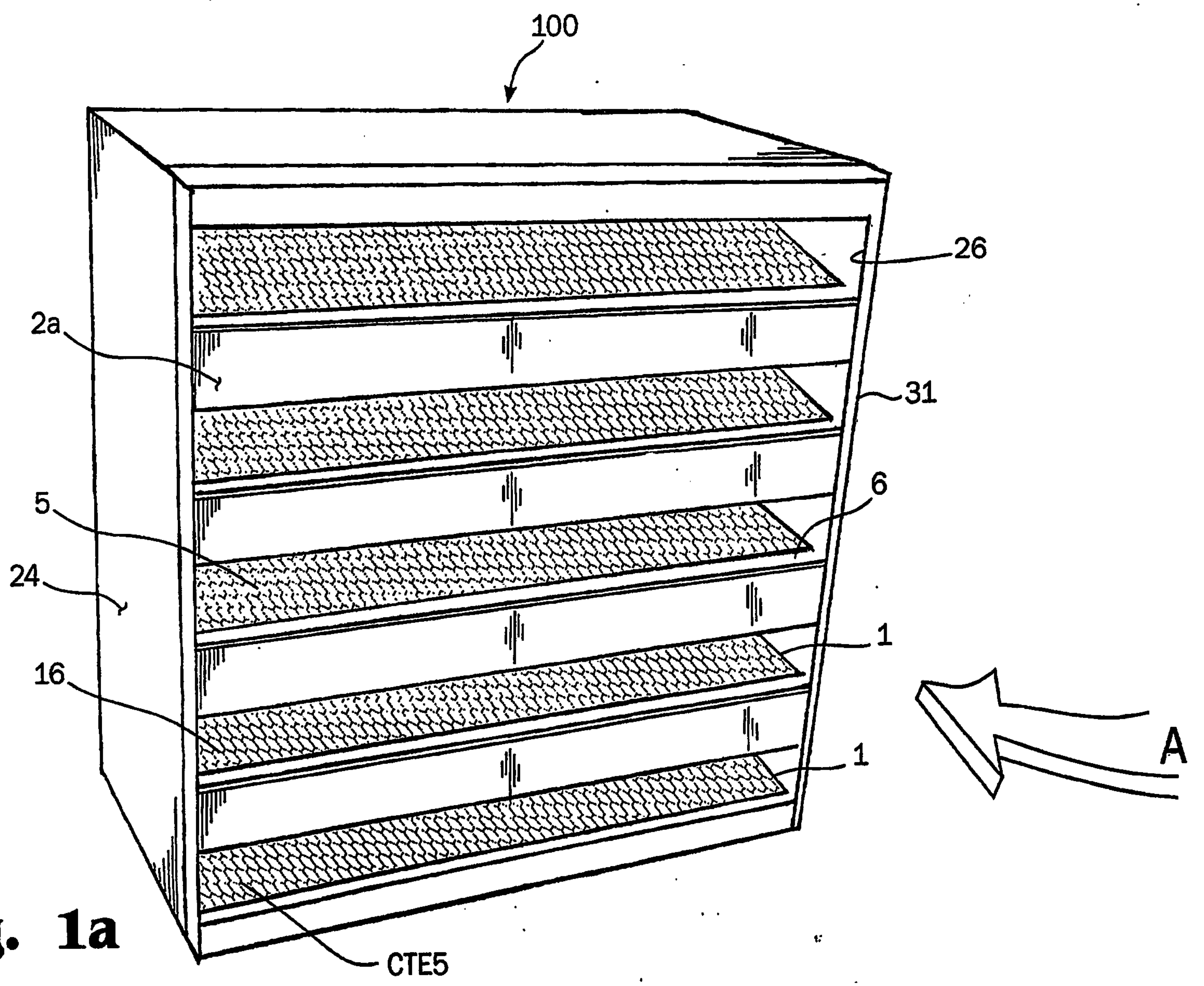

Fig. 1a

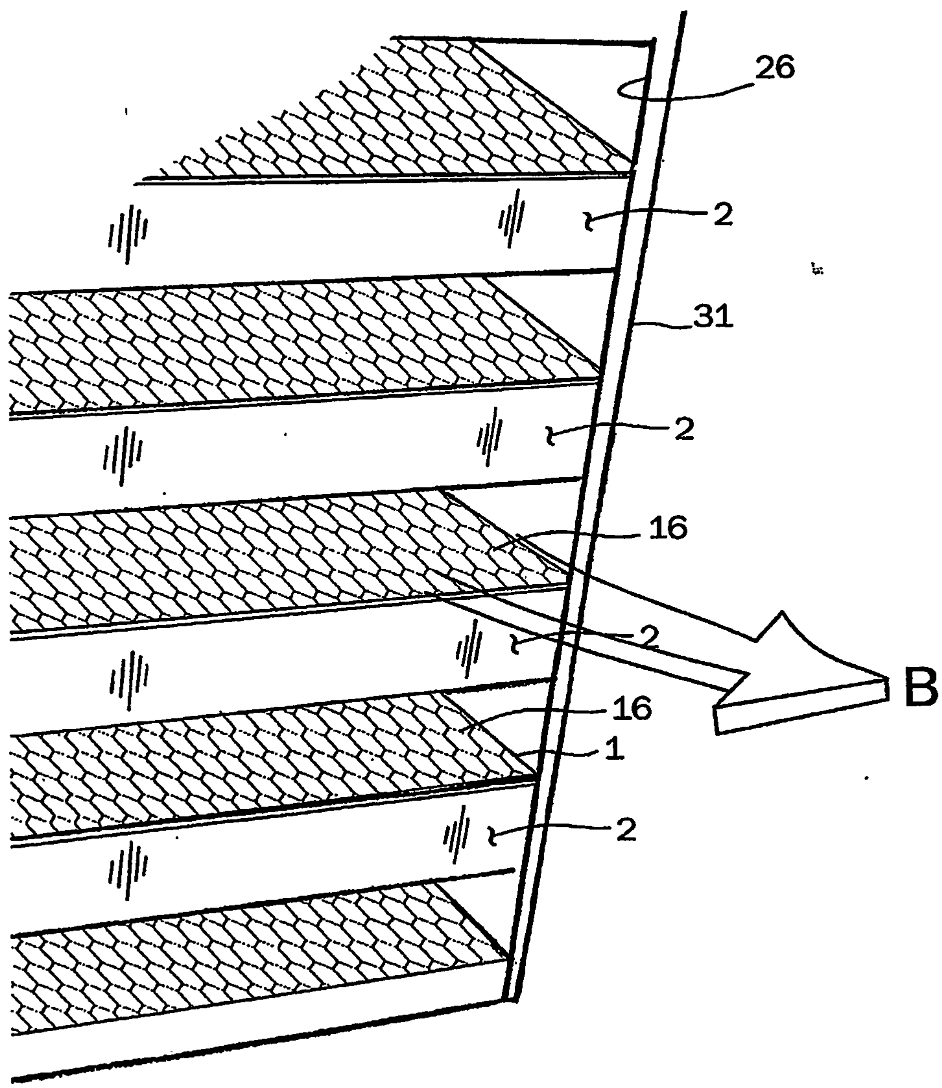

Fig. 1b

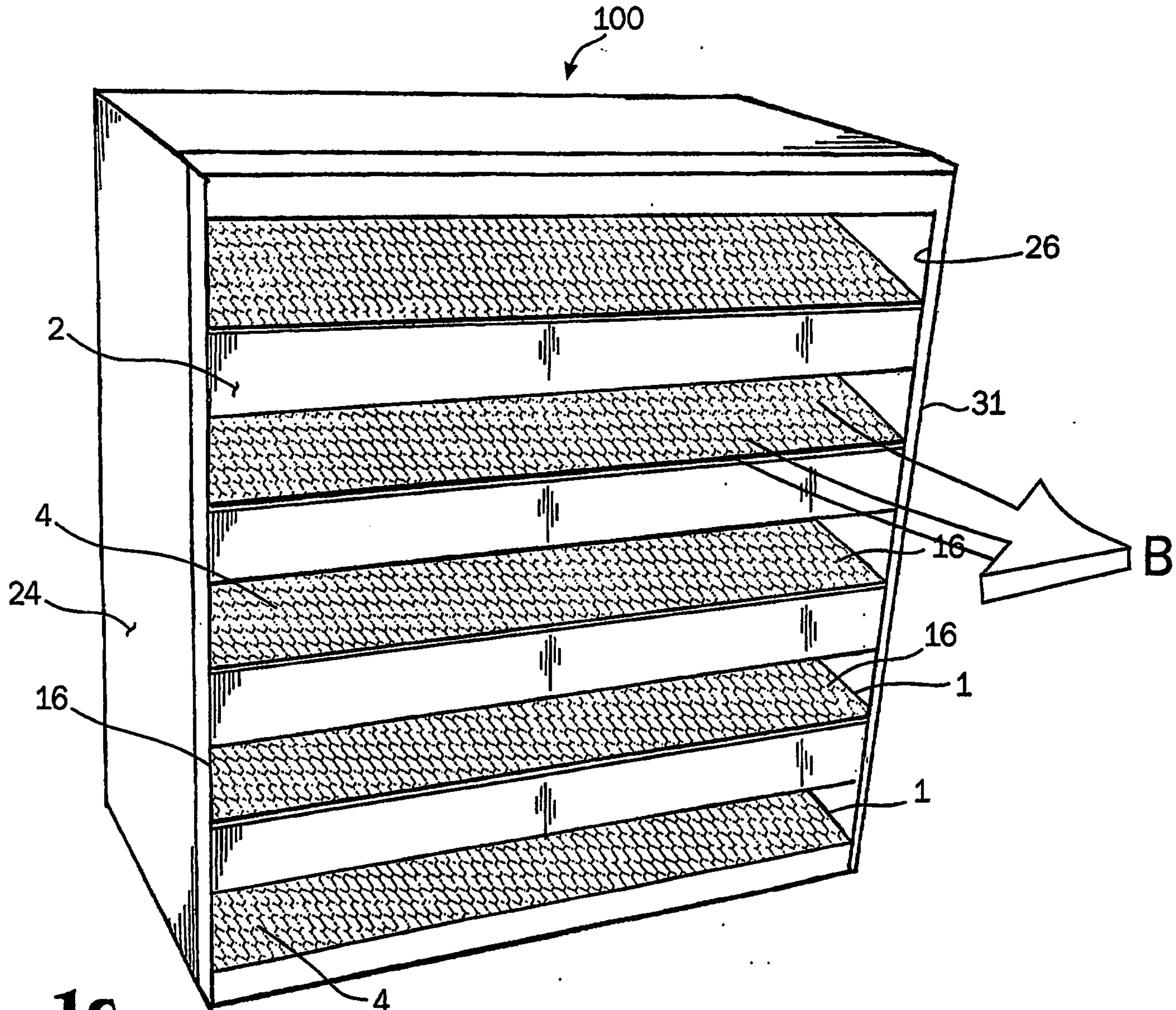

Fig. 1c

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Fig. 2

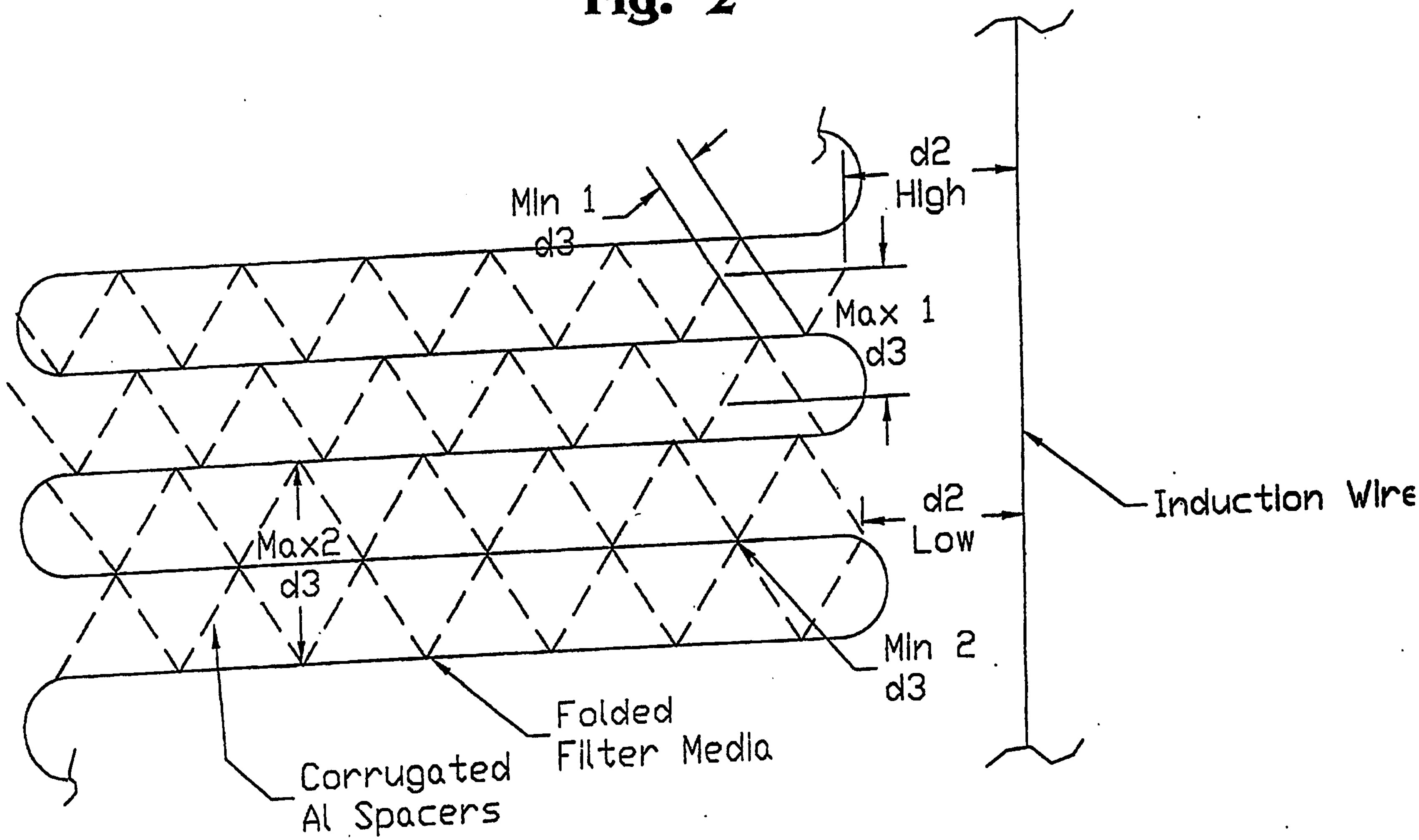
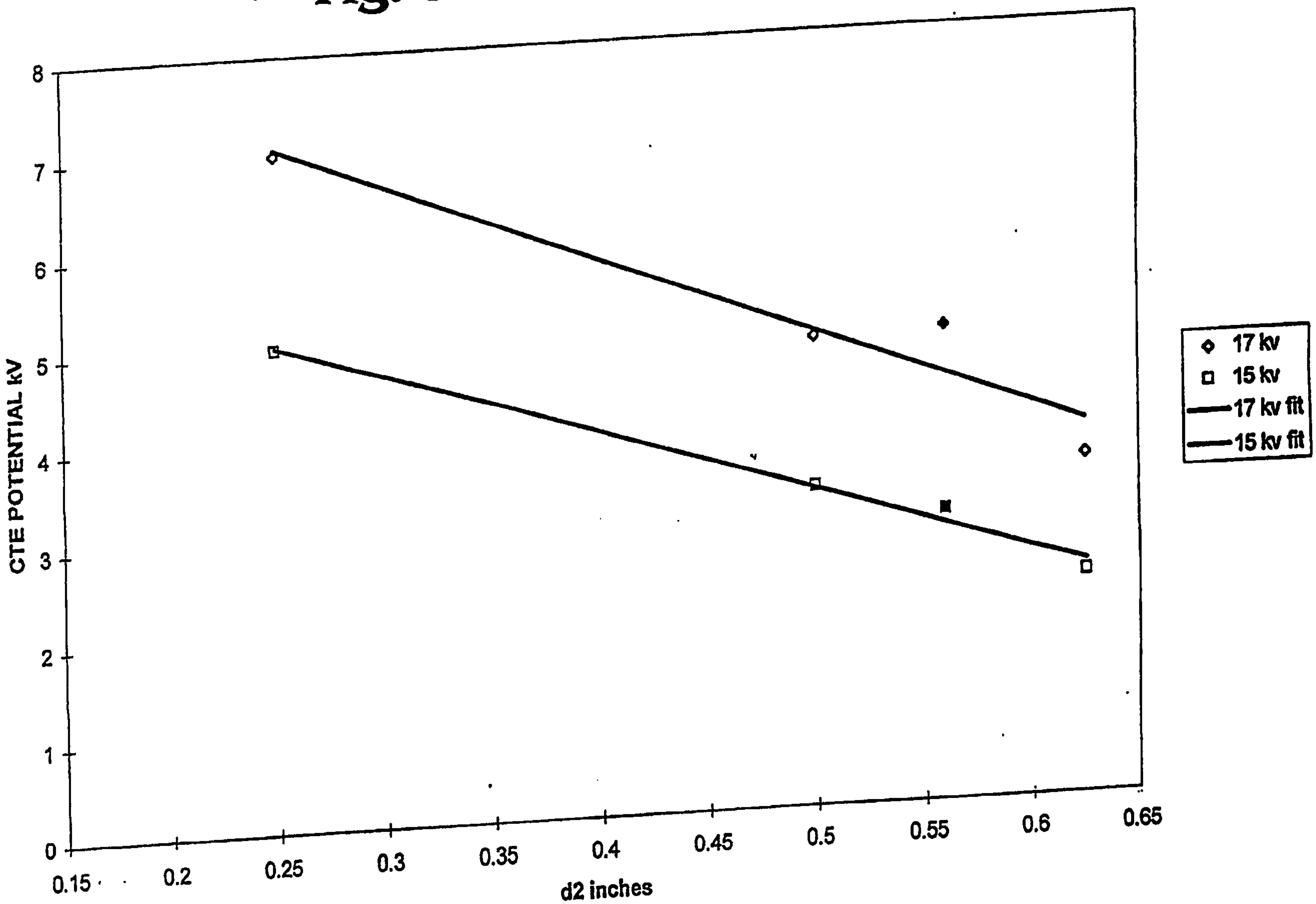


Fig. 3


CTE POTENTIAL kV
0
1
2
3
4
5
6
7
8
0.15
0.2
0.25
0.3
0.35
0.4
0.45
0.5
0.55
0.6
0.65
d2 inches
17 kv
15 kv
17 kv fit
15 kv fit

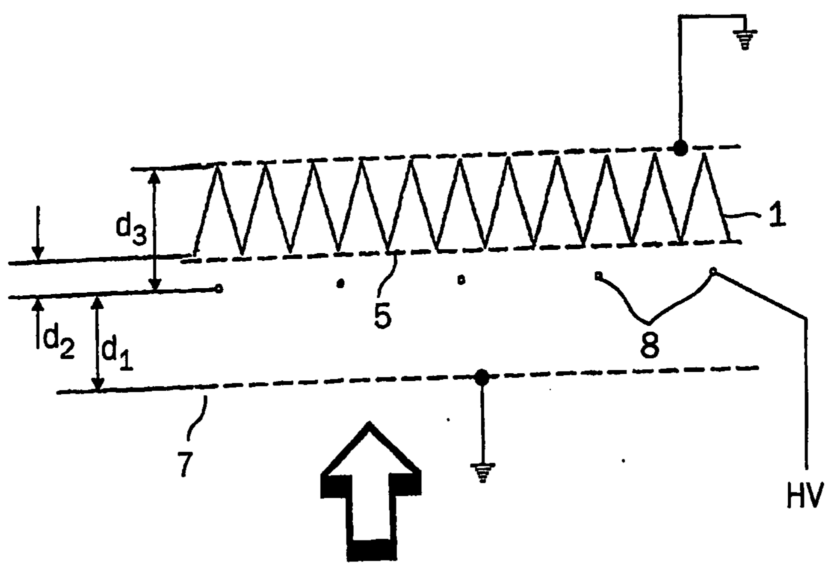


Fig. 4

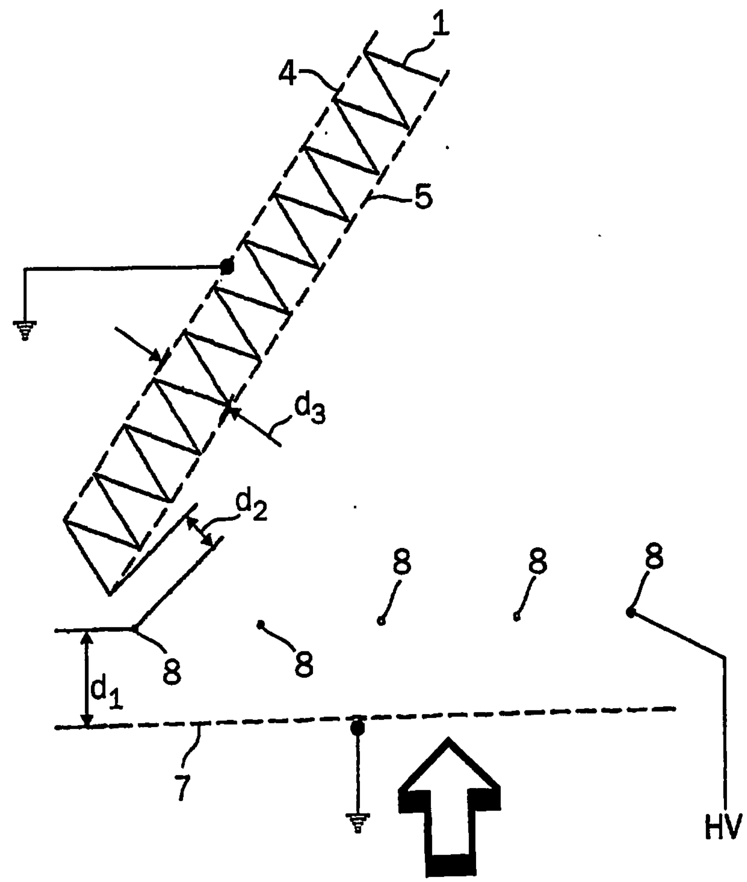
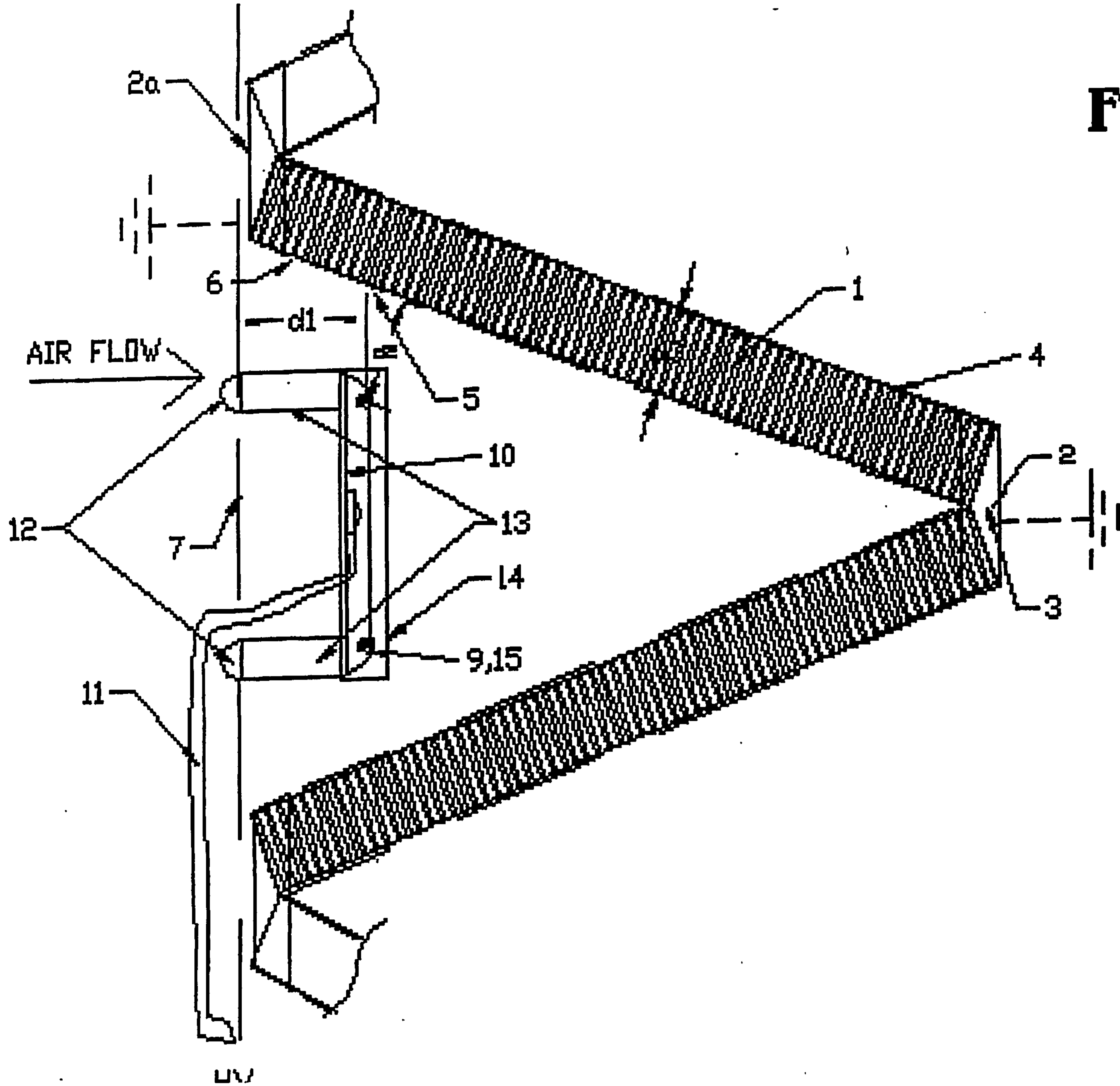


Fig. 5

Fig. 6



Isometric Blowup of Ionizer Assembly

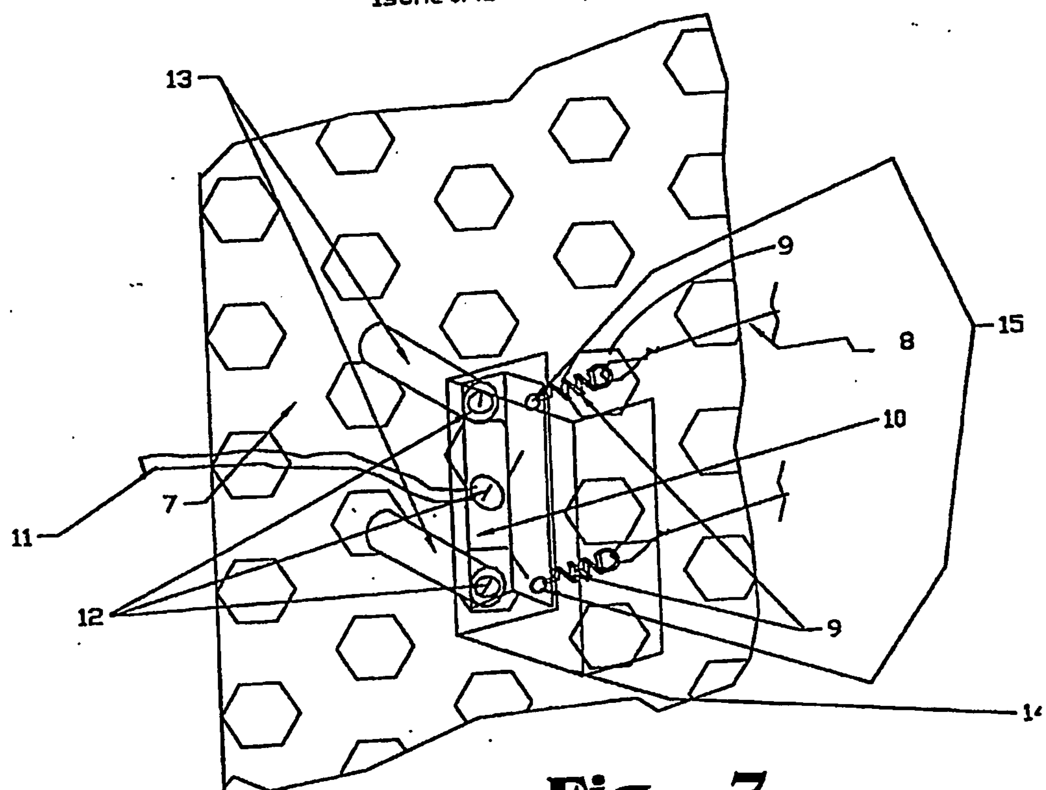


Fig. 7

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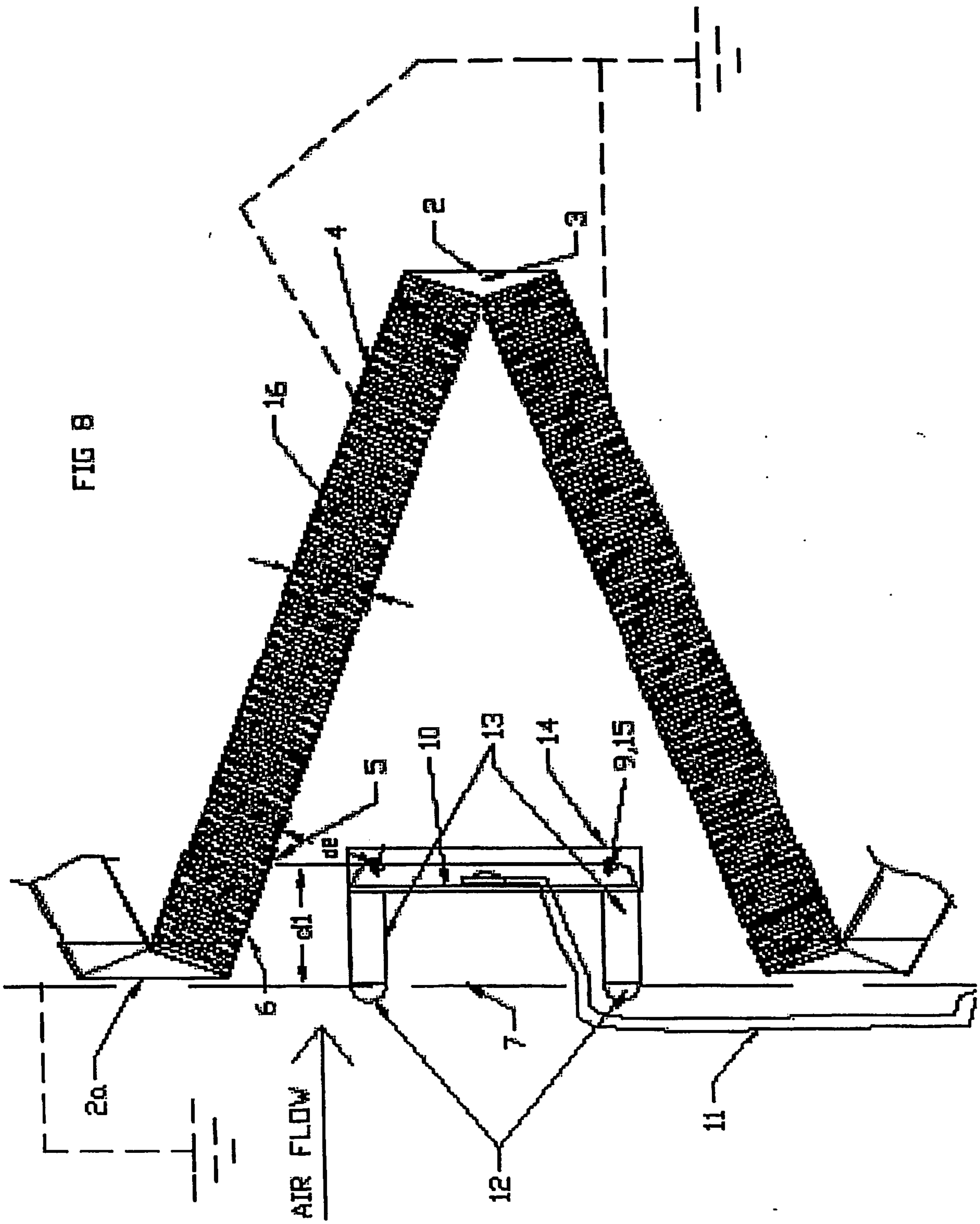


FIG 8

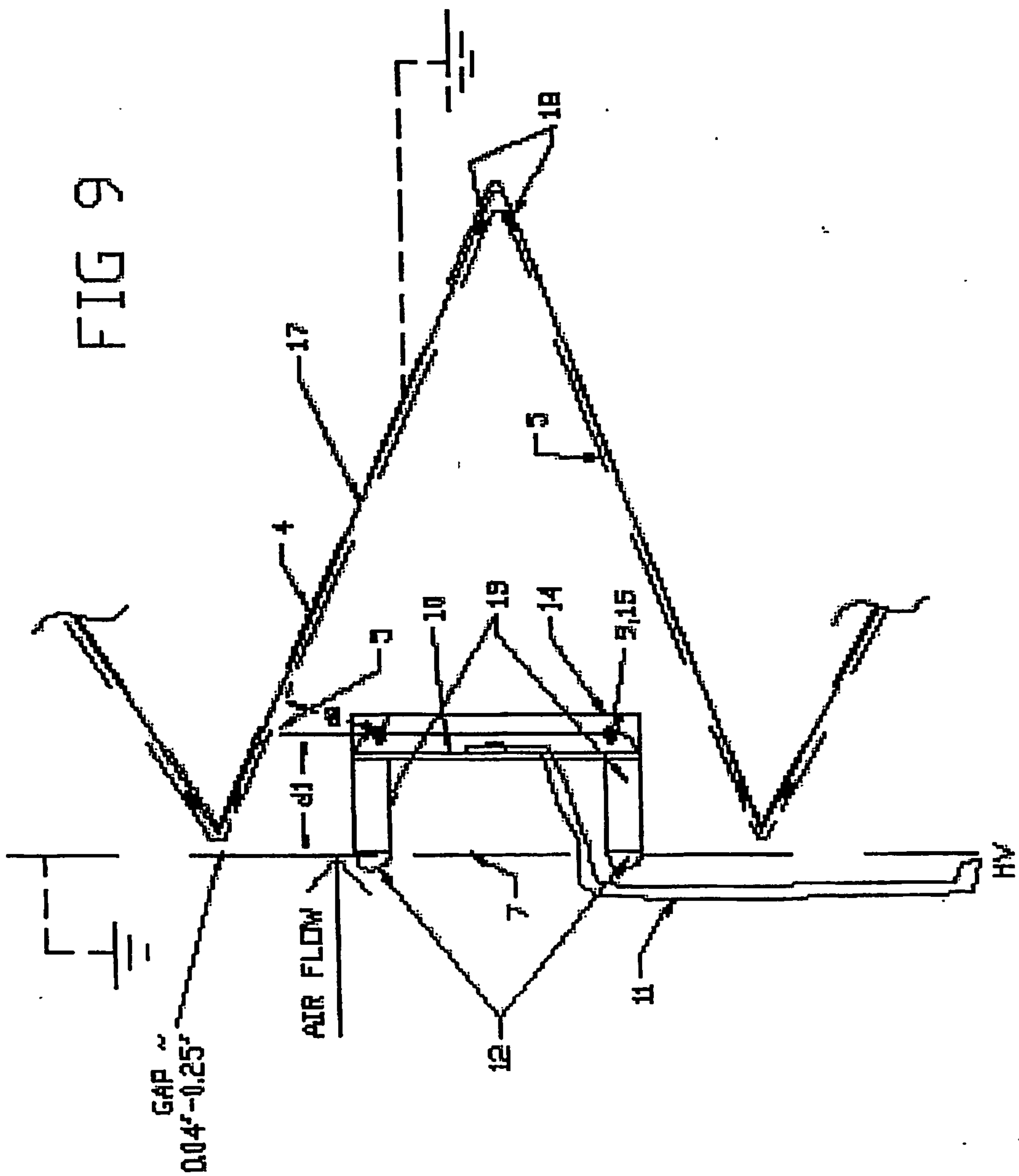
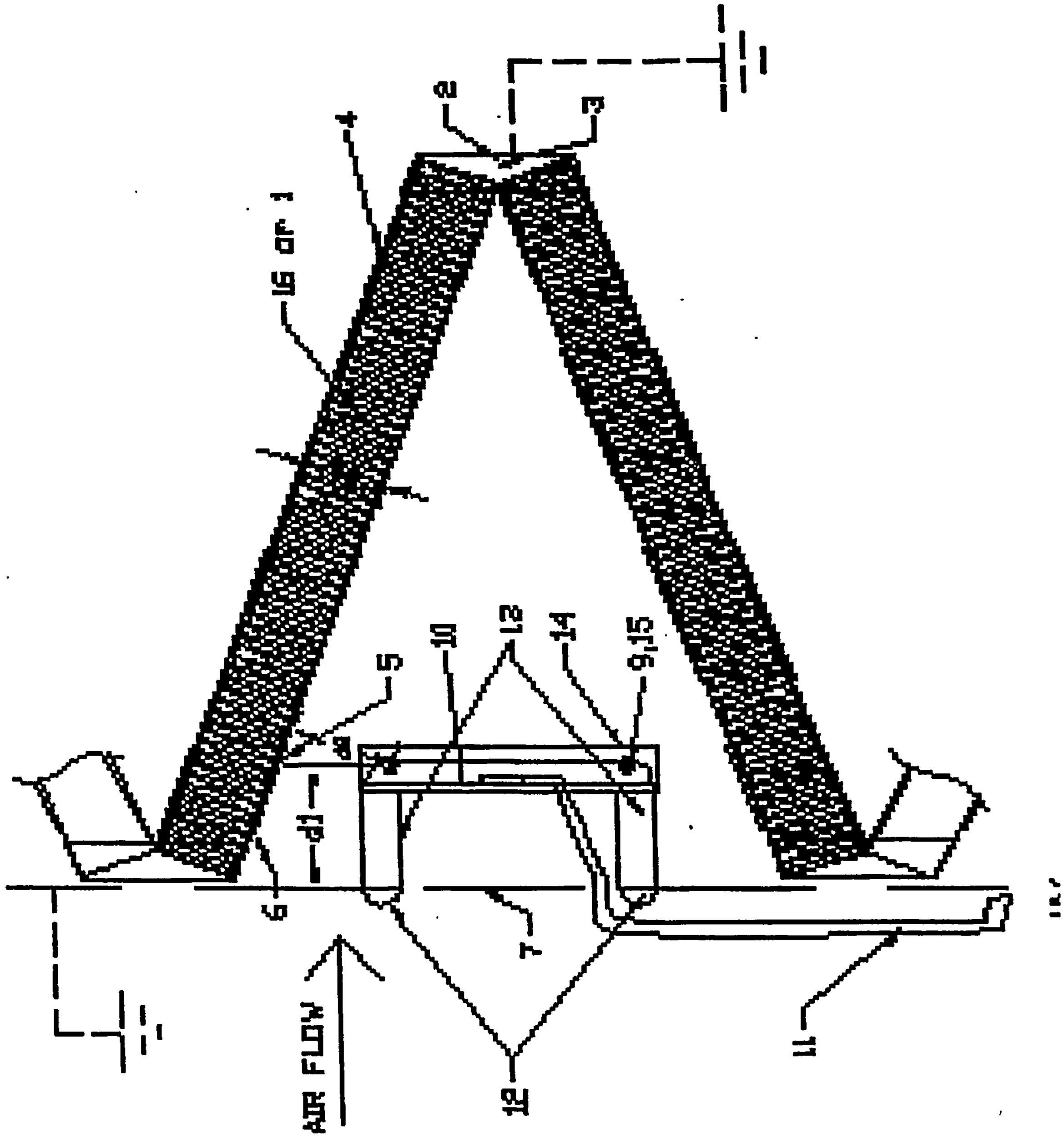


FIG 9

Fig 10



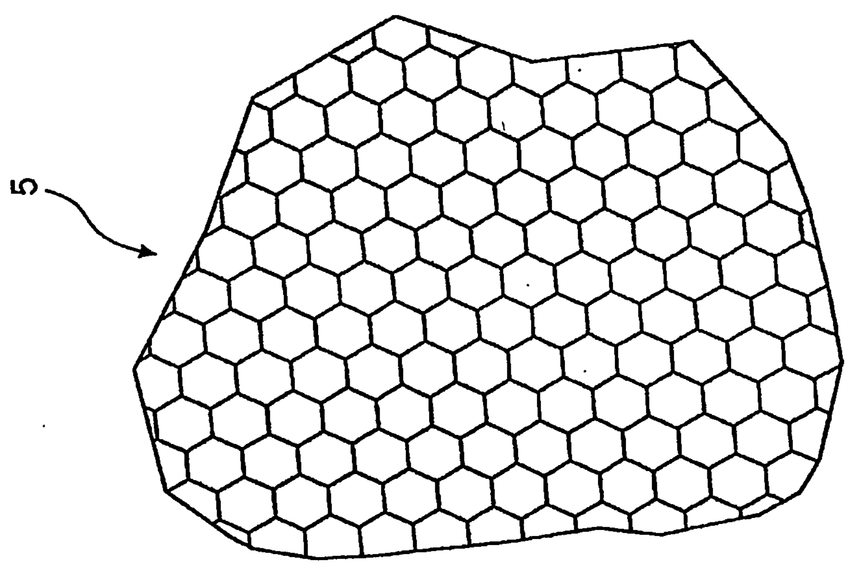


Fig. 11

Fig 12

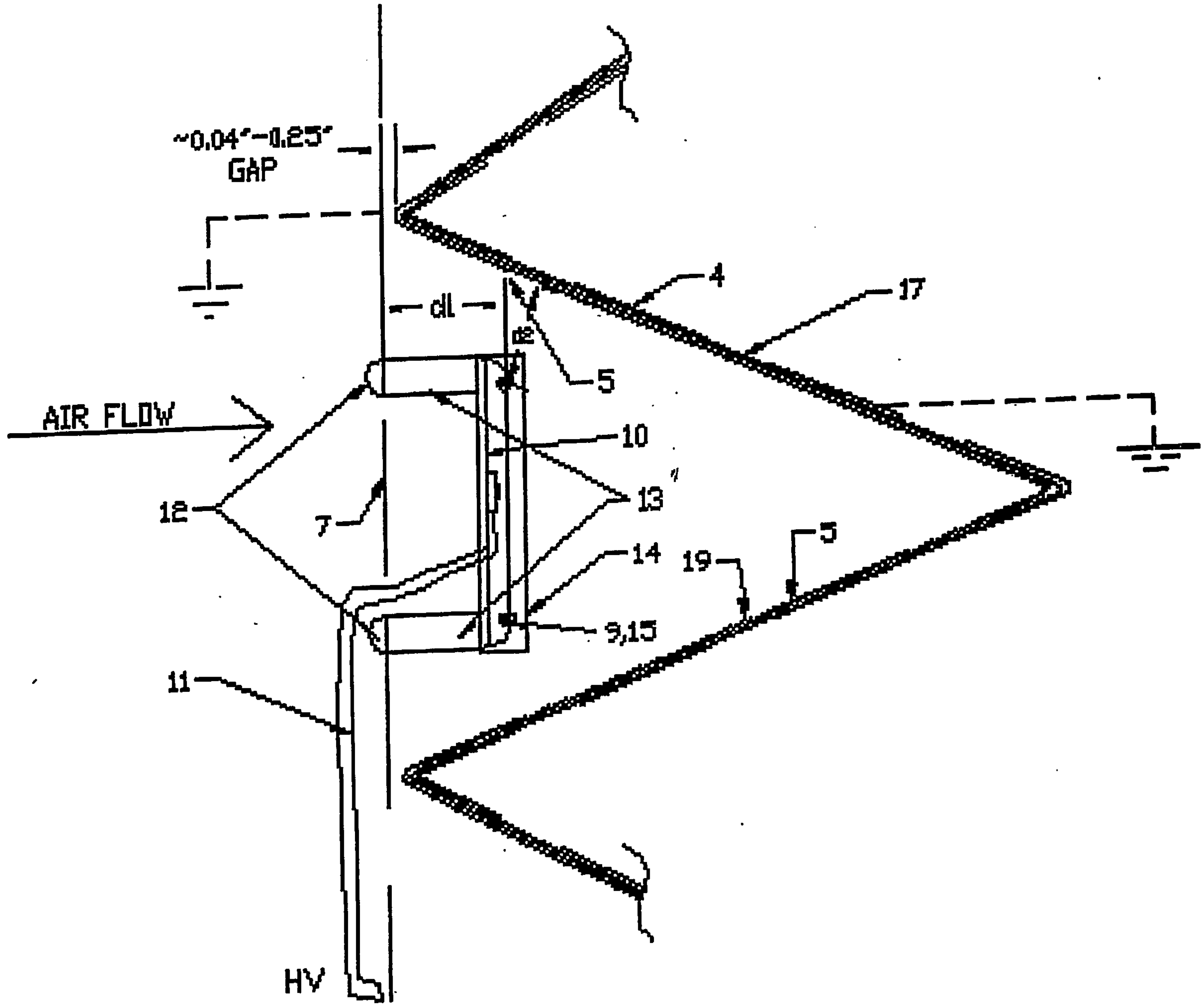


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FIG 13

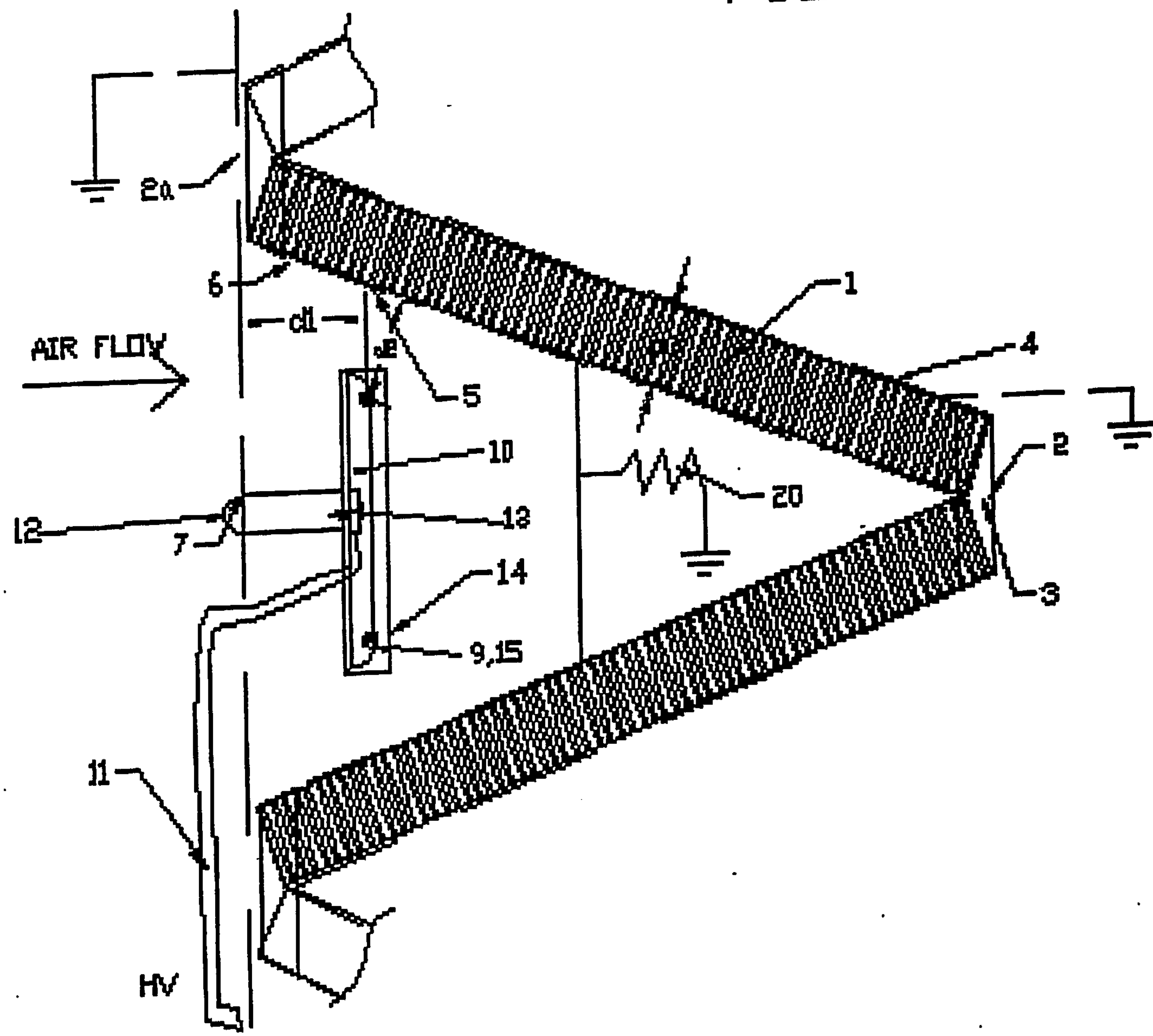
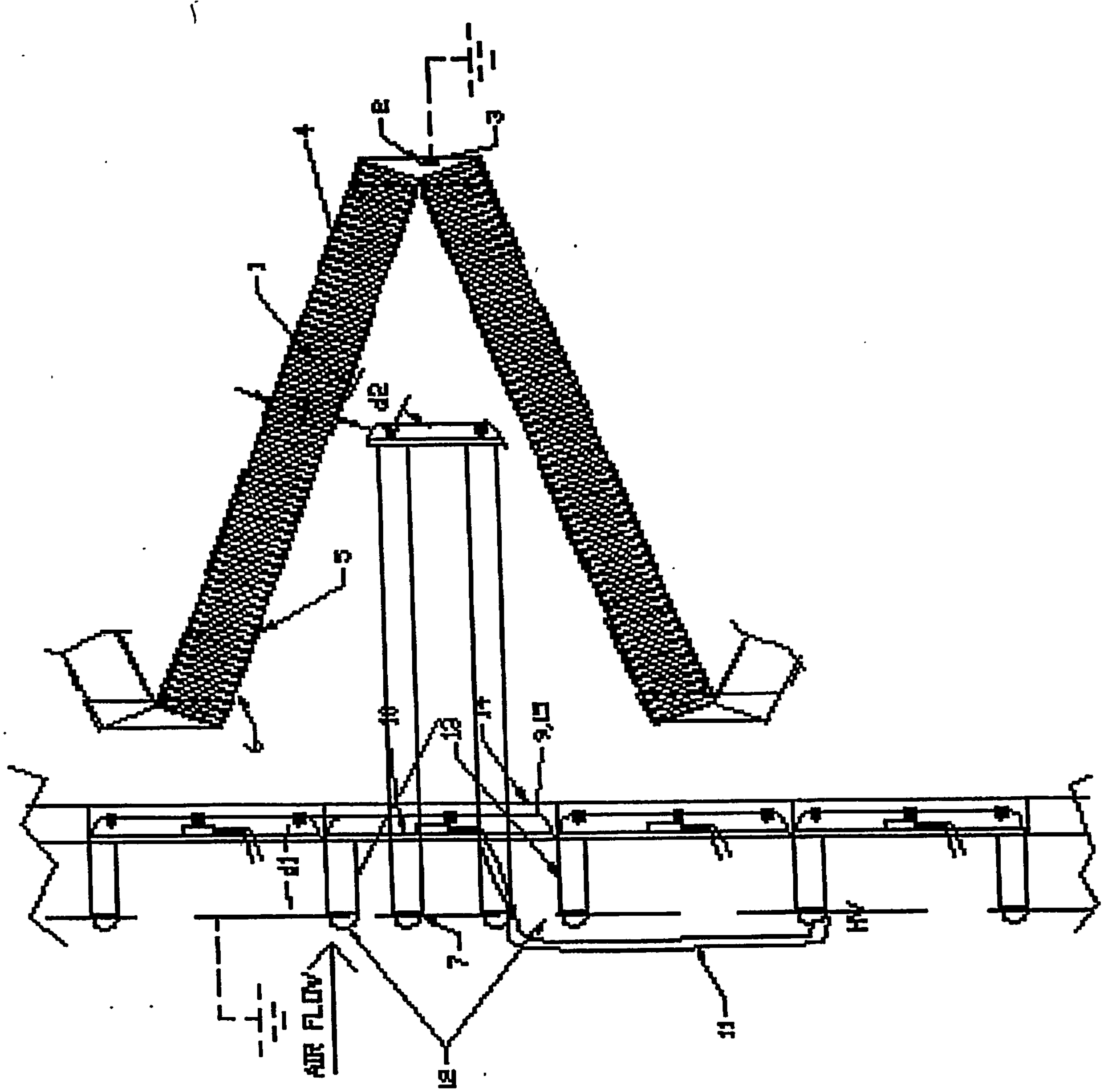


FIG 14



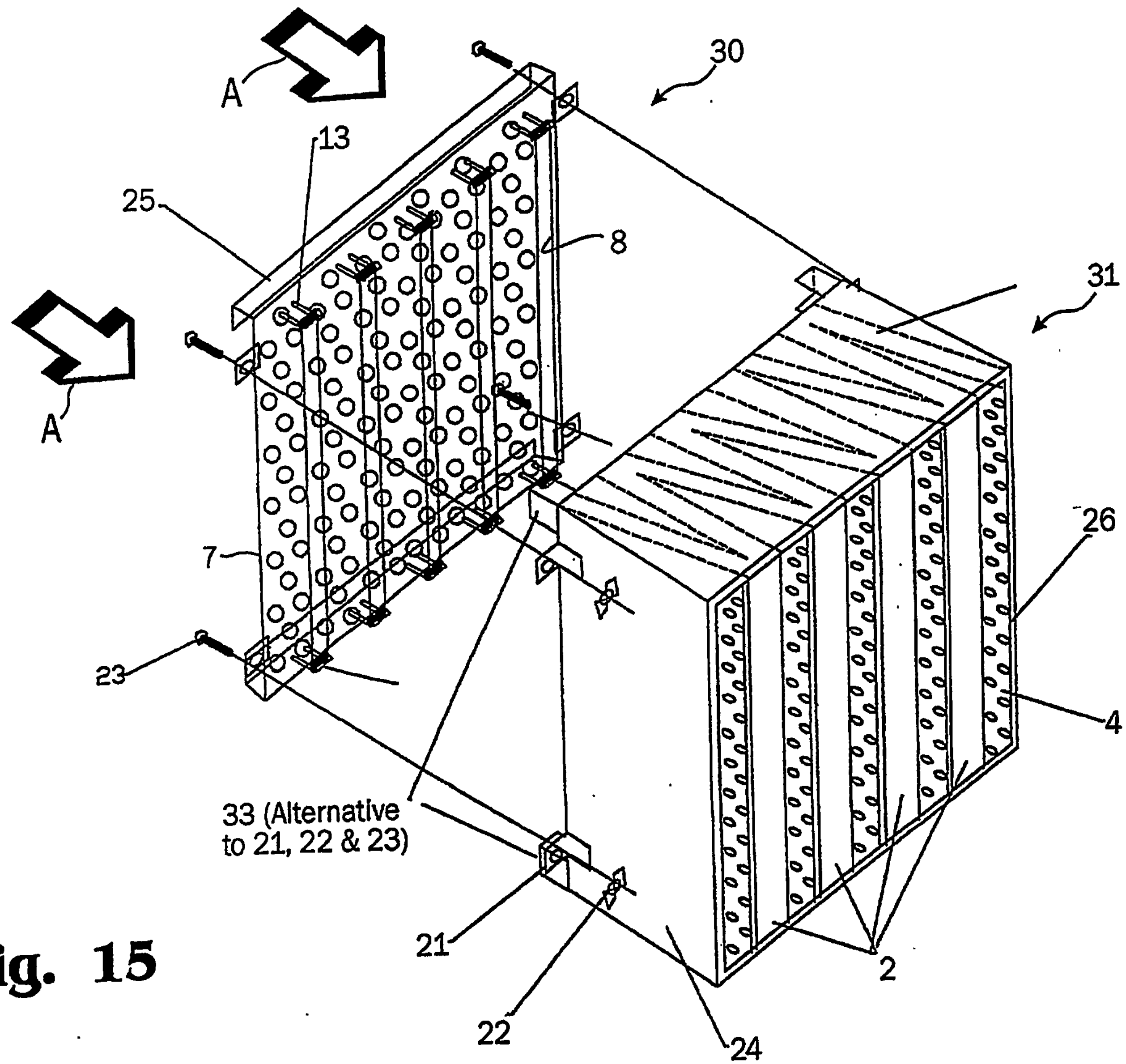
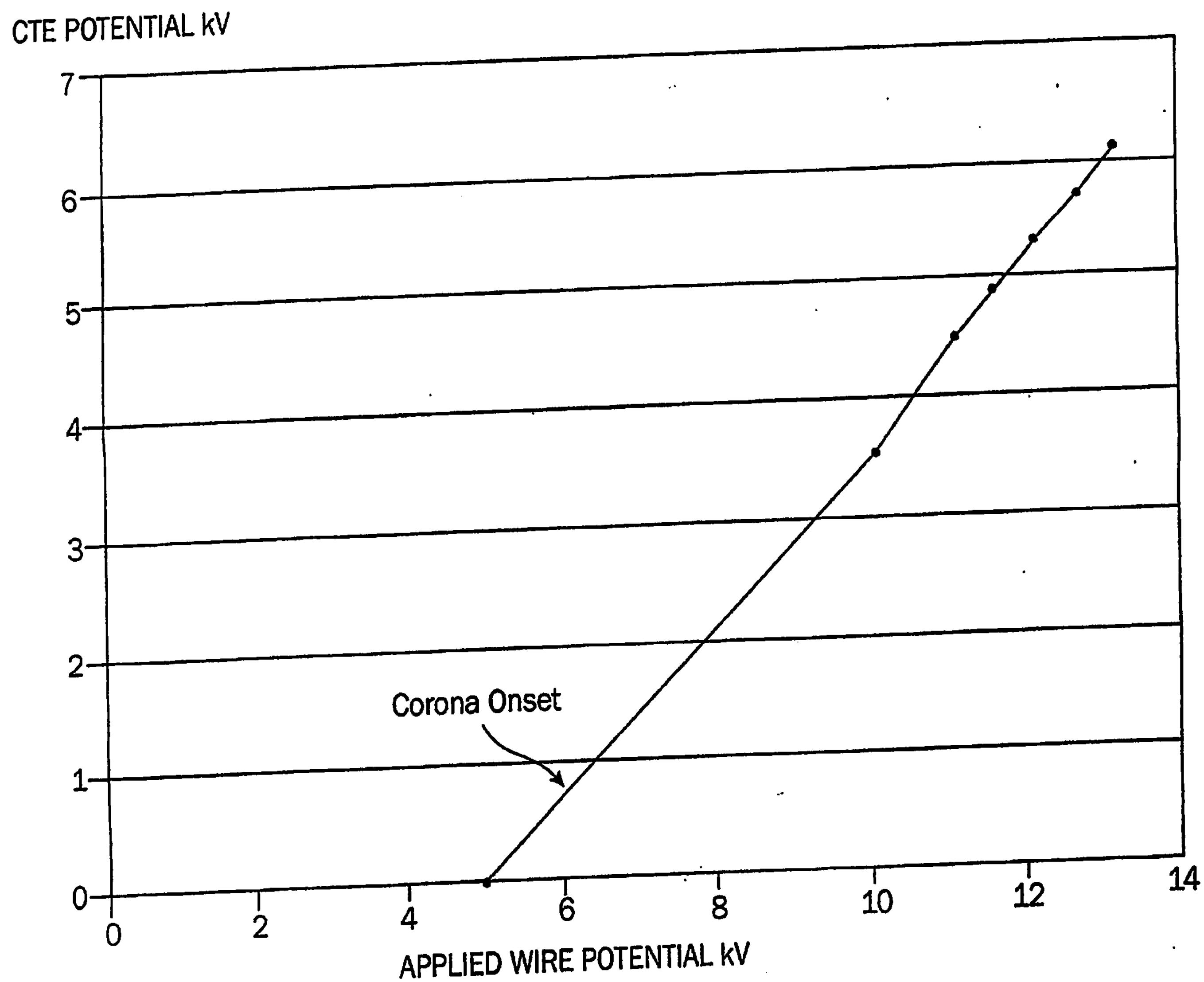


Fig. 15

Fig. 16



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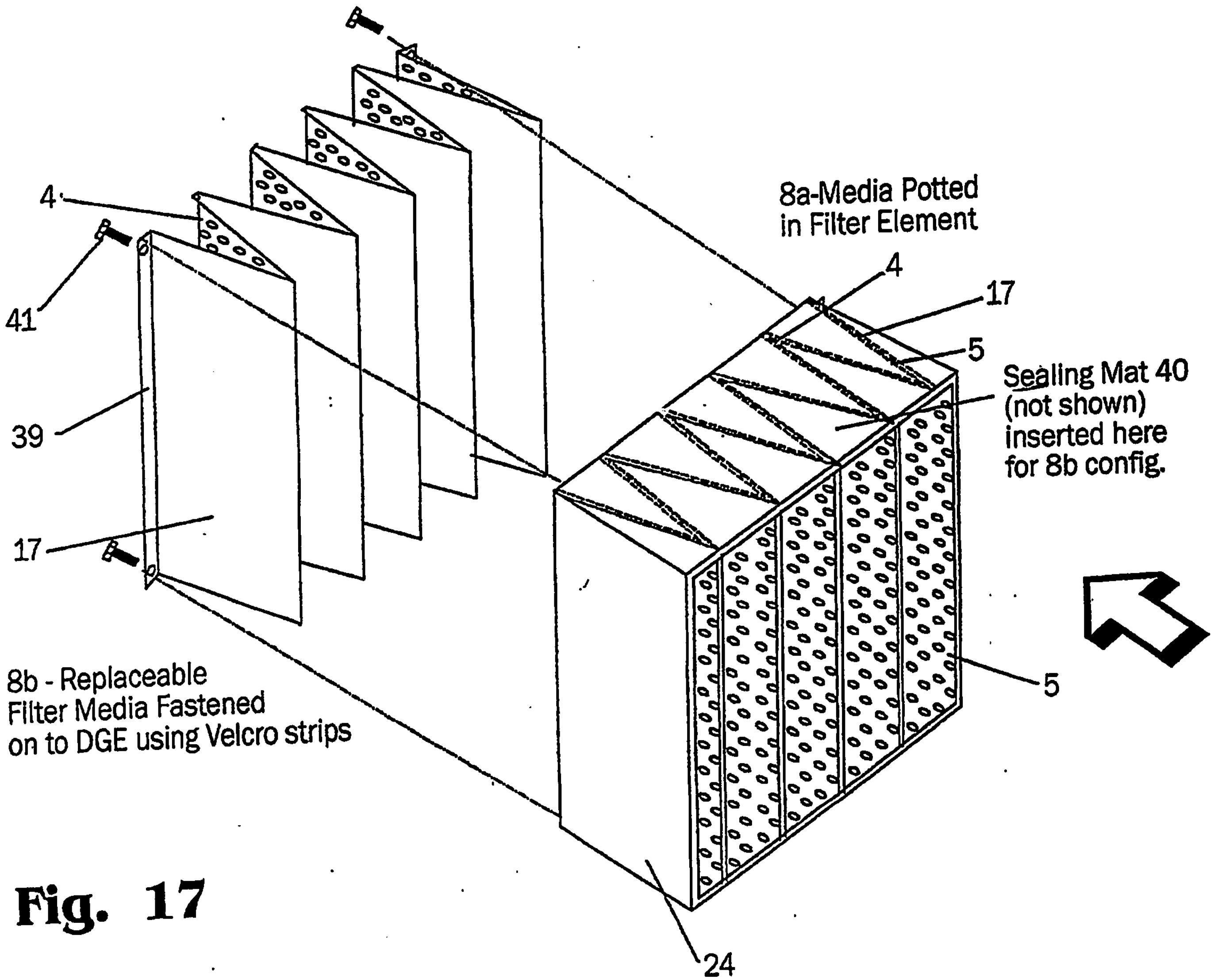
8a-Media Potted
in Filter Element
4
17
5
Sealing Mat 40
(not shown)
inserted here
for 8b config.
5
24
4
41
39
17
8b - Replaceable
Filter Media Fastened
on to DGE using Velcro strips

Fig. 17

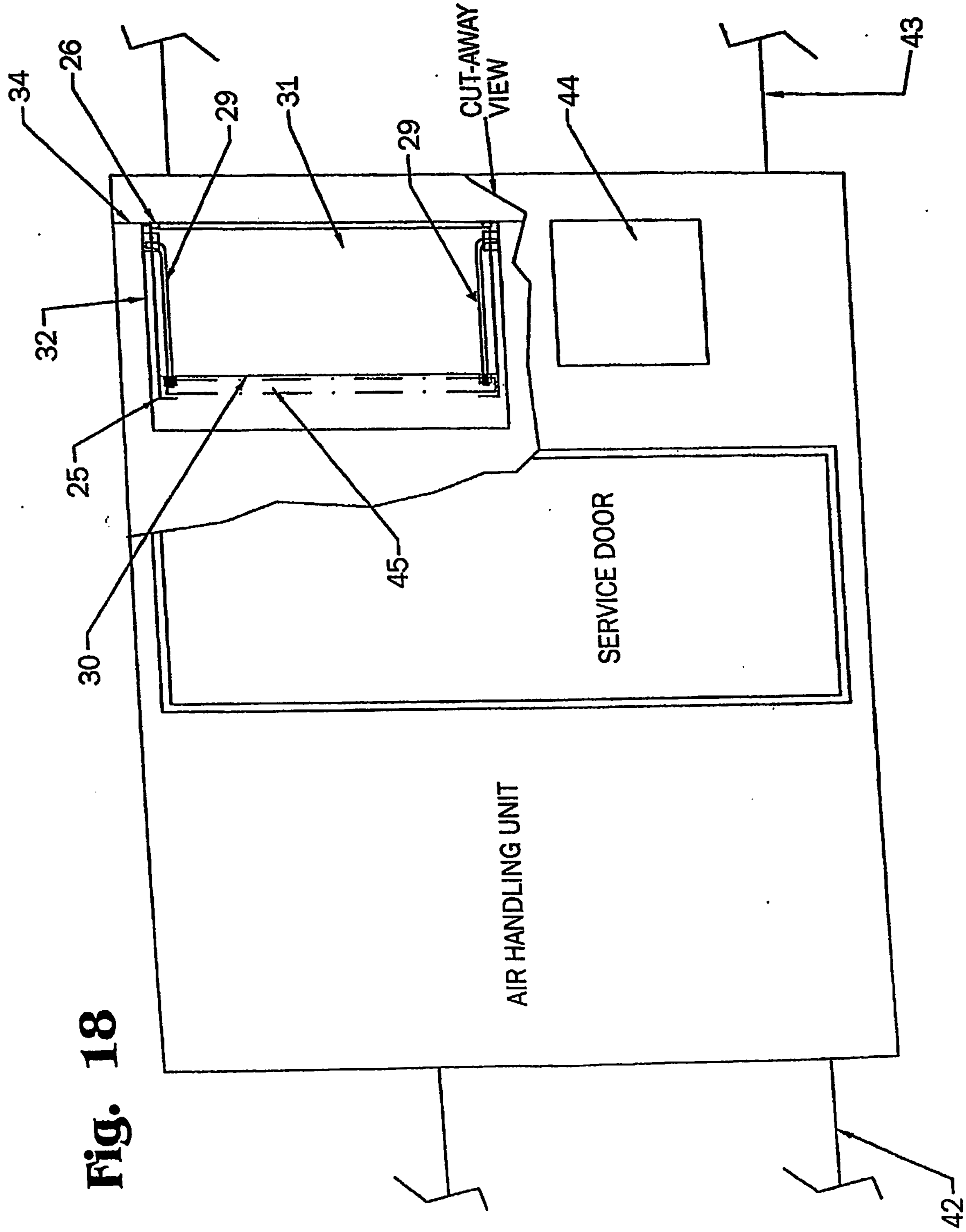
34
26
29
31
CUT-AWAY VIEW
44
43
32
29
25
45
30
SERVICE DOOR
AIR HANDLING UNIT
42

Fig. 18

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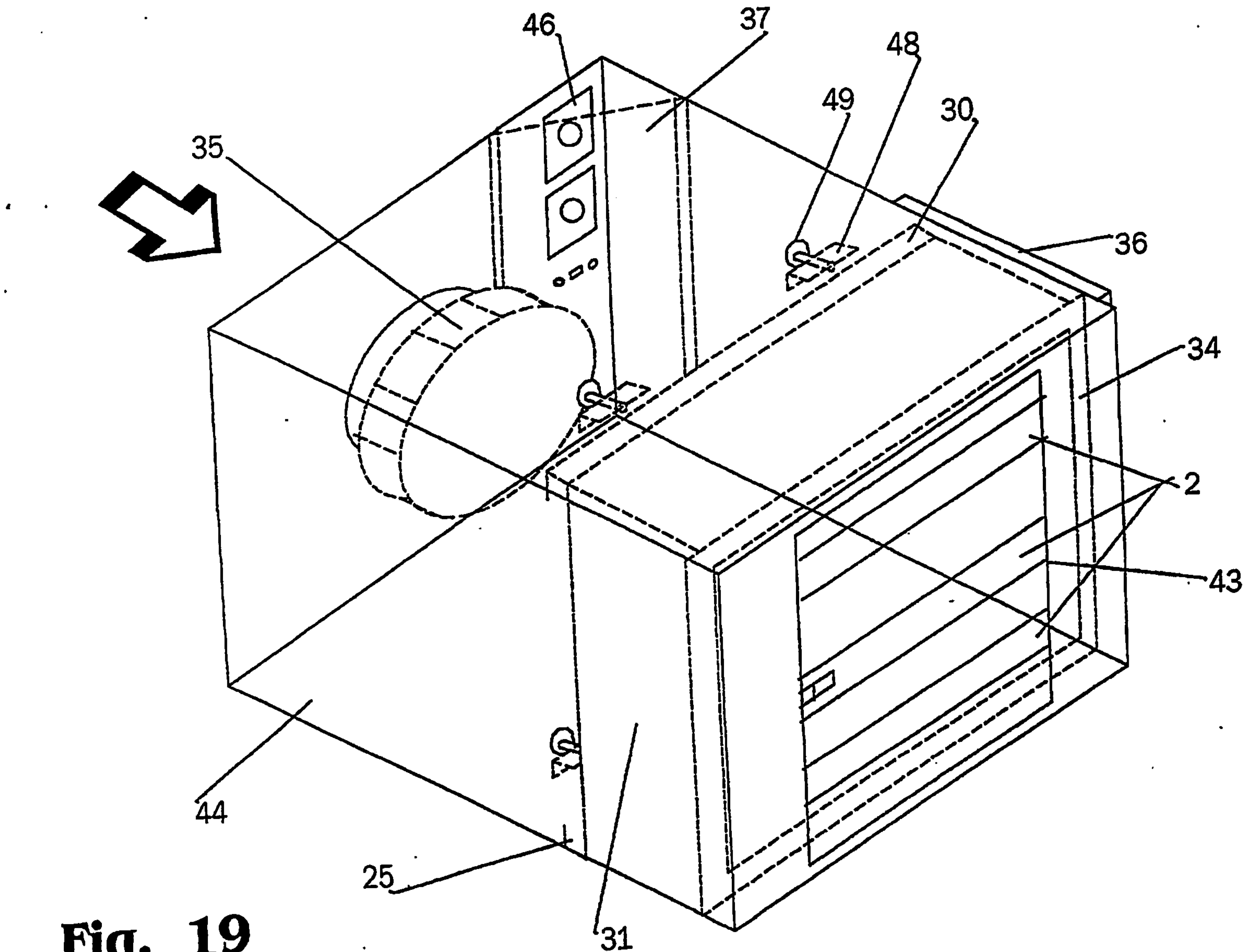

Fig. 19